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NATIONAL DAM SAFETY PROGRAM. UNNAMED TRIBUTARY TO HARMON CREEK, --ETC(U)
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PA 485

MOI No. PA 01123 Pennider No. 63-81 SCS No. PA 485

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PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM



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DEPARTMENT OF THE ARMY Baltimore District, Corps of Engineers

Baltimore, Maryland 21203

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PA-465
WASHINGTON COUNTY, COMMONWEALTH OF PENNSYLVANIA
NDI No. PA 01123
PennDER No. 63-81
SCS No. PA 485

PHASE I INSPECTION REPORT

NATIONAL DAM SAFETY PROGRAM.

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Prepared for: DEPARTMENT OF THE ARMY
Baltimore District, Corps of Engineers
Baltimore, Maryland 21203

Prepared by: MICHAEL BAKER, JR., INC.
Consulting Engineers
4301 Dutch Ridge Road
Beaver, Pennsylvania 15009

(10) John A. Fiziubeki

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PREFACE

This report is prepared under guidance contained in the "Recommended Guidelines for Safety Inspection of Dams," for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

PA 485, Washington County, Pennsylvania NDI No. 01123, PennDER No. 63-81, SCS No. PA 485 Unnamed Tributary to Harmon Creek Inspected 20 March 1980

ASSESSMENT OF GENERAL CONDITIONS

PA 485 is classified as an "Intermediate" size - "High" hazard dam. The dam, owned by the Washington County Commissioners, is used to reduce floodwater damages in the Harmon Creek Watershed. The dam and appurtenant structures were found to be in good condition at the time of the inspection.

Hydrologic/hydraulic evaluations, performed in accordance with procedures established by the Baltimore District, U.S. Army Corps of Engineers, for Phase I Inspection Reports, revealed that the spillway will pass the Probable Maximum Flood (PMF) without overtopping the dam. A spillway design flood (SDF) equal to the PMF is required for PA 485. The spillway is therefore considered to be "adequate".

The visual inspection revealed several minor deficiencies which require remedial action by the owners of the dam:

- Remove the debris which has collected in the trash rack in front of the low-level intake on the riser unit.
- 2) Repair the minor tire rutting along the crest of the dam. Vehicles should be prevented from traveling along the dam crest.
- 3) Reseed the areas along the dam crest and the berm on the upstream face of the dam where vegetation is sparse.
- 4) Repair the erosion gulley on the downstream side of the dam along the junction of the embankment and right abutment.
- 5) Regrade the berms on the downstream face of the embankment to provide better surface drainage.

It is also recommended that the slide in the left abutment immediately upstream from the emergency spillway be monitored during future inspections to ensure that this does not become a significant problem.

In addition, the following operational measures are recommended to be undertaken by the owner:

- 1) Develop a detailed emergency operation and warning system.
- During periods of unusually heavy rainfall, provide around-the-clock surveillance of the dam. 2)
- When warning of a storm of major proportions is 3) given by the National Weather Service, the owner should activate the emergency operation and warning system.

Submitted by:

MICHAEL BAKER, JR., INC.

John A. Dziubek, P.E. Engineering Manager-Geotechnical

Date: 10 July 1980

Approved by:

DEPARTMENT OF THE ARMY

BALTIMORE DISTRICT, CORPS OF ENGINEERS

JAMES W. PECK

Colonel, Corps of Engineers District Engineer

Date: 1/August 80



Overall View of Upstream Face of Dam from Reservoir Area



Overall View of Crest of Dam and Downsteam Face from Right Abutment

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM PA 485

NDI No. PA 01123, PennDER No. 63-81, SCS No. PA 485

SECTION 1 - PROJECT INFORMATION

1.1 GENERAL

- a. Authority The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. Purpose of Inspection The purpose of inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 DESCRIPTION OF PROJECT

Description of Dam and Appurtenances - PA 485 is a zoned earthfill embankment with a total length of 630 feet, including the emergency spillway on the left abutment. The minimum top of dam elevation is 931.8 feet Mean Sea Level (M.S.L.). The height and crest width of the embankment are 78 feet and 14 feet, respectively. The upstream face of the embankment has a slope of 3H:1V (Horizontal to Vertical) with a 40 foot wide bench located between Elevation 880.3 feet M.S.L. and Elevation 884.3 feet M.S.L. The downstream face of the embankment has a slope of 2.5H:lV. There are two benches on the downstream face; the first is 10 feet wide and is located between Elevation 895.0 feet M.S.L. and Elevation 896.0 feet M.S.L.; the second is 20 feet wide and lies between Elevation 883.0 feet M.S.L. and 885.0 feet M.S.L.1

The embankment was constructed using three zones of fill material. The inner core of the dam, zone I, consists of fine-grained, relatively impervious material. The core section has 1.5H:1V side slopes to Elevation 917.7 feet M.S.L. Above this point, the core extends vertically to within 5 feet of the crest of the dam. The width of this vertical section is 14 feet. The outer shell of

The two benches on the downstream side of the embankment have a l percent slope down towards the right abutment. Elevations listed above correspond to the elevations of the benches at Stations 3+12 on the top of dam profile included in Appendix A.

the embankment, zone II, was constructed using weathered siltstone and silty sand. Additional fill, zone III, was placed at the upstream and downstream toe of the embankment. This material consists of crushed rock excavated from the emergency spillway, cut-off trench, principal spillway, and left abutment.

A cut-off trench with a minimum depth of 3 feet, side slopes of 2H:1V, and a bottom width ranging from 12 feet to 22 feet extends under the entire length of the embankment. Zone I material was used to backfill the cut-off trench.

The drainage system for the dam has four components: (1) a foundation drain, (2) a chimney drain, (3) a rock face blanket drain, and (4) an outlet blanket drain. The foundation drain consists of a 12 inch perforated drain pipe and graded drain fill. extends from the base of the left abutment to normal pool level on the right abutment. chimney drain is located on the downstream side of the embankment between the zone I and zone II This drain material is 10 feet thick. does not cover the full length of the embankment, rather, it is divided into two sections which extend approximately 75 feet out from each abutment. The chimney drain outlets into the foundation Drainage for the left abutment is provided drain. by a rock face blanket drain which consists of a blanket of coarse aggregate approximately 8.5 feet This drain outlets into the outlet blanket drain which extends from the junction of the chimney drain and the base of the left abutment to the downstream toe of the embankment.

Rock gutters have been placed at the junctions of the embankment and abutments to provide surface drainage.

The principal spillway is a drop-inlet structure consisting of a two stage reinforced concrete riser connected to a 30 inch diameter reinforced concrete outlet pipe. The low-level inlet on the riser unit is a 1.5 foot wide by 1.0 foot high orifice with an invert elevation of 879.5 feet M.S.L. This orifice maintains the normal pool level at Elevation 879.5 feet M.S.L. The upper-level inlet consists of two concrete overflow weirs with rounded downstream edges. The weirs are located on either side of the riser unit. Each is 7.5 feet long and has a crest elevation of

895.5 feet M.S.L. There is a rectangular opening 7.5 feet wide and 1.25 feet high above each weir. The openings to the low-level and upper-level inlets are protected by metal trash racks.

The outlet pipe from the riser unit is 484 feet long and has 15 concrete anti-seep collars. The pipe exits into a concrete impact basin at the downstream toe of the embankment.

The reservoir drain consists of a trapezoidal channel leading from the reservoir area to a 30 inch diameter opening at the base of the riser unit. The channel is 3.5 feet deep, 30.6 feet wide, and has lH:lV side slopes. The invert elevation of the drain opening at the base of the riser unit is 855.5 feet M.S.L. The reservoir can be drawn down by opening the 30 inch gate valve which covers this opening. The controls for the gate valve are located on the top of the riser unit.

The emergency spillway for the dam is located at the left abutment. It consists of a vegetated trapezoidal channel with a bottom width of 50 feet and 2H:lV side slopes. The spillway was designed as an earth and rock cut in the left abutment of the dam. The control section in the spillway, located approximately along the centerline of the crest of the dam, is at Elevation 917.7 feet M.S.L. Downstream from the emergency spillway is a 5 foot high protection dike (see Plates 3 and 5 for details).

- b. Location PA 485 is located on an unnamed tributary to Harmon Creek, 175 feet north of Township Route T-819 in Washington County, Pennsylvania. The dam is approximately 1.5 miles northwest of Eldersville. Pennsylvania. The dam and reservoir can be found on the Steubenville East, West Virginia-Pennsylvania-Ohio 7.5 minute USGS topographic quadrangle.
- c. <u>Size Classification</u> The dam is 78 feet high and has a storage capacity of 951.8 acre-feet. The dam is therefore in the "Intermediate" size category.
- d. <u>Hazard Classification</u> There are two homes located immediately downstream from the dam. Loss of life in these structures during a dam failure is believed likely to occur. The dam is therefore in the "High" hazard category.

- e. Ownership The dam is owned by the Washington County Commissioners, Washington County Courthouse, Washington, Pennsylvania.
- f. Purpose of Dam PA 485 is one of several floodwater retarding dams constructed by the U.S. Department of Agriculture, Soil Conservation Service (SCS) in the Harmon Creek Watershed. Its purpose is to reduce floodwater damages in the downstream areas of the watershed.
- g. Design and Construction History The dam was designed by the SCS in 1975. Construction was begun in April 1976 and completed in October 1977. The contractor responsible for construction of the dam was Solomon-Teslovich of Masontown, Pennsylvania.
- h. Normal Operating Procedures The reservoir level is typically maintained by the low-level inlet on the riser unit at Elevation 879.5 feet M.S.L. Washington County and SCS personnel inspect the dam each year according to the procedures for annual inspections of SCS dams of this type.

1.3 PERTINENT DATA

a.	Drainage Area	(square miles) -	2.18
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b. <u>Discharge at Dam Site (c.f.s.)</u> -

Peak Outflow at -	
Crest of Riser (El. 895.5 ft. M.S.L.) -	28.5
Crest of Emergency Spillway (El.	
917.7 ft. M.S.L.) -	132
Design High Water (El. 920.9 ft. M.S.L.) -	825
Top of Dam (El. 931.2 ft. M.S.L.) -	8693
Maximum Known Non-Damaging Discharge -	120

c. Elevation (feet above M.S.L.) -

Design Top of Dam -	931.2
Design High Water -	920.9
Crest of Emergency Spillway -	917.7
Crest of Upper-Level Inlet -	895.5
Invert of Low-Level Inlet -	879.5
Normal (Sediment) Pool -	879.5
Streambed at Downstream Toe -	853 <u>+</u>

d. <u>Reservoir (feet)</u> -

Length of Normal Pool (El. 879.5 ft. M.S.L.) - 1800 Length of Maximum Pool (El. 931.2 ft. M.S.L.) - 5350

e. Storage (acre-feet) -

Normal Pool (El. 879.5 ft. M.S.L.) - 43.5²
Crest of Emergency Spillway (El. 917.7 ft. M.S.L.) - 536.8
Design High Water (El. 920.9 ft. M.S.L.) - 621.8
Top of Dam (El. 931.2 ft. M.S.L.) - 951.8

f. Reservoir Surface (acres) -

Normal Pool (El. 879.5 ft. M.S.L.) - 5.7 Crest of Emergency Spillway (El. 917.7 ft. 25.5 M.S.L.) - 25.5 Design High Water (El. 920.9 ft. M.S.L.) - 27.7 Top of Dam (El. 931.2 ft. M.S.L.) - 37.0

g. Dam -

Type - Zoned earthfill embankment

Length (feet) - 630

Height (feet) - 78

Crest Width (feet) - 14

Slopes - Upstream - 3H: LV with a 40 foot wide bench between El. 880.3 ft. and 884.3 ft.

M.S.L.

Downstream - 2.5H:1V with a 10 foot wide bench between El. 895.0 ft. and 896.0 ft M.S.L. and a 20 foot wide bench between El. 883.0 ft. and 885.0 ft. M.S.L.

Zoning - The embankment was constructed using three zones of fill material. The fine-grained, impervious inner core, zone I, has 1.5H:lV side slopes to El. 917.7 ft. M.S.L. Above this point, the core extends vertically to within 5 feet of the crest of the dam. The outer shell of the embankment, zone II, was constructed using weathered siltstone and silty sand. Additional fill, zone III, consisting of crushed rock from the various excavations, was placed at the upstream and downstream toe of the embankment (see Plate 5 for details).

This volume is reserved for a 50-year accumulation of sediment. It is not included in floodwater storage calculations.

- Cut-off There is a cut-off trench with a minimum depth of 3 feet, side slopes of 2H:1V, and a bottom width ranging from 12 feet to 22 feet along the centerline of the embankment.
- Drains A foundation drain, a chimney drain, a rock face blanket drain at the left abutment, and an outlet blanket drain have been included in the dam.

Grout Curtain - None

h. Diversion and Regulatory Tunnel -

None

- i. Spillway (Emergency Spillway) -
 - Type Vegetated trapezoidal earth and rock cut channel at the left abutment

Length Along Centerline (feet) -	440
Bottom Width (feet) -	50
Side Slopes -	2H:1V
Crest Elevation (feet M.S.L.) -	917.7

j. Regulatory Outlets (Principal Spillway) - The principal spillway is a standard SCS two stage covered riser unit. The low-level inlet is a 1.5 foot wide by 1.0 foot high orifice with an invert elevation of 879.5 ft. M.S.L. The upper-level inlet consists of two concrete overflow weirs with a total weir length of 15 feet. The crest of the upper-level inlet is at El. 895.5 ft. M.S.L.

The outlet pipe from the riser unit is a 30 inch diameter reinforced concrete pipe 484 feet long. This pipe exits into a concrete impact basin at the downstream toe of the embankment.

The reservoir drain consists of a 30 inch diameter opening at the base of the riser unit (invert El. 855.5 ft. M.S.L.). The drain is controlled by a 30 inch gate valve operated from the top of the riser unit.

SECTION 2 - ENGINEERING DATA

2.1 DESIGN

PA 485 was designed as a single purpose floodwater retarding structure. It is one of several flood control dams constructed by the SCS in the Harmon Creek Watershed to reduce flood damages in the lower reaches of the basin. The dam was designed to retard the 100-year frequency storm without discharge occurring in the emergency spillway.

PA 485 was designed by the SCS according to its standard procedures for structures of this type. Design data reviewed for this report included the following:

- 1) SCS Drawings No. PA-485-P, "Harmon Creek Watershed Project, Brooke and Hancock Counties, West Virginia, Washington County, Pennsylvania, Floodwater Retarding Dam PA-485," 52 sheets "as built" 12 October 1977.
- 2) "Design Report, Site PA-485, Pennsylvania," U.S. Department of Agriculture, Soil Conservation Service, undated (copy obtained from Harrisburg office of the SCS).
- 3) Inspection reports filed by the Pennsylvania Department of Environmental Resources' (PennDER) personnel during construction of the dam (from 16 April 1976 to 17 October 1977).
- 4) The permit application and various pieces of correspondence contained in the PennDER file on the dam.
- 5) The "Erosion and Sediment Control Plan" prepared by the SCS office in Washington, Pennsylvania for this dam.

2.2 CONSTRUCTION

The construction of PA 485 was performed by Solomon-Teslovich of Masontown, Pennsylvania. Construction was begun in April 1976 and completed in October 1977. No mention of significant problems during construction is made in any of the available information.

2.3 OPERATION

The reservoir level is typically maintained by the low-level inlet of the riser unit at Elevation 879.5 feet M.S.L. Washington County and SCS personnel inspect the dam each year according to the procedures for annual inspections of SCS dams of this type.

2.4 EVALUATION

- a. Availability The information reviewed is readily available from the PennDER file on the dam and from the SCS office in Harrisburg, Pennsylvania.
- b. Adequacy The information available is adequate for a Phase I Inspection of this dam.
- c. <u>Validity</u> There is no reason at the present time to question the validity of the available information.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

- a. General The visual inspection was performed on 20 March 1980. No unusual weather conditions were experienced and the reservoir was 2.8 feet above normal pool. The dam and appurtenances were found to be in good condition at the time of the inspection. Noteworthy observations made during the visual inspection are described in the following paragraphs. The complete visual inspection check list, field sketch³, top of dam profile, and typical crosssection are presented in Appendix A.
- b. Dam The following is a list of the minor deficiencies observed during the visual inspection of the embankment and abutments.
 - 1) There is some minor tire rutting along the crest of the embankment from vehicles being driven over the dam. Measures should be taken to prevent vehicles from driving on the embankment.
 - 2) Vegetation is relatively sparse in several areas on the dam crest and on the berm on the upstream face of the embankment. These areas should be reseeded.
 - 3) There is a small slide on the left abutment upstream of the emergency spillway. This slide does not represent a significant problem to the embankment or the emergency spillway at the present time.
 - 4) Some water has collected on the berms on the downstream face of the dam. These areas are above the reservoir level which indicates that the water is probably the result of recent precipitation and not seepage through the embankment.

³Stationing on the field sketch prepared for this report is different than that shown on SCS design plans included as plates in Appendix E. Any references made to stationing in this report refer to the stations shown on the field sketch and not those on the SCS design drawings.

(Note: During the field review a small mud slide was observed on the left abutment adjacent to the downstream rock gutter approximately 30 feet downstream from the crest. This slide does not affect the structural stability but may clog the rock gutter with soil.)

- 5) A small erosion gulley has developed on the downstream side of the dam along the junction of the embankment and right abutment.
- c. Appurtenant Structures A small amount of debris has collected in the trash rack protecting the low-level inlet. A small amount of water has collected in the upstream section of the emergency spillway. This water is probably the result of recent precipitation. No other problems in the appurtenant structures were observed.
- d. Reservoir Area The reservoir slopes are primarily forested and relatively steep. The small slide mentioned in Section 3.1.b., item 3 was the only evidence of slope instability observed during the inspection.

The dam was designed with a sediment storage capacity equivalent to 50-years of sediment accumulation. There was no indication that sedimentation was occurring at a rate faster than that anticipated by the SCS in the design of this dam.

e. Downstream Channel - A board approximately 1.0 foot high has been placed across the bottom of the outlet channel approximately 150 feet downstream from the impact basin. A fence also crosses over the channel at this point. Debris collecting in the fence and the board combine to back up water in the outlet channel, forming a small pool approximately 2 feet deep. It appears that this pool was created to provide an area for geese. The backwater from this pool reaches the impact basin but does not represent a significant restriction to flow out of the outlet channel.

The outlet channel passes under Township Route T-819 approximately 175 feet downstream from the impact basin. Flow is carried under this road by an opening 5 feet high by 20 feet long. Immediately downstream from this road are two residential structures. The next structures are located approximately 2000 feet further downstream on Harmon Creek.

SECTION 4 - OPERATIONAL PROCEDURES

4.1 PROCEDURES

The dam and appurtenances are inspected by Washington County and SCS personnel each year according to the procedures for annual inspections of SCS dams of this type. Formal maintenance and inspection procedures are presented in the "Erosion and Sediment Control Plan" for this dam.

4.2 MAINTENANCE OF DAM AND APPURTENANCES

Routine maintenance is performed periodically by Washington County personnel. Formal maintenance procedures are described in the "Erosion and Sediment Control Plan" for this dam. At the present time, maintenance of the dam and appurtenances is considered to be adequate.

4.3 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT

An emergency warning procedure is being developed for PA 485. However, at the present time, no formal procedure is in effect.

4.4 EVALUATION OF OPERATIONAL ADEQUACY

The present operational and maintenance procedures for the dam are considered to be adequate. Formal emergency warning procedures should be developed and implemented.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 EVALUATION OF FEATURES

a. Design Data - Hydrologic and hydraulic design calculations for PA 485 were obtained from the SCS design report for this dam. The dam was built as part of a system to reduce floodwater damages in the downstream reaches of the Harmon Creek Watershed. It was designed to retard the 100-year frequency storm without discharge occurring in the emergency spillway. A sediment storage volume equivalent to a 50-year accumulation of sediment has been provided.

The elevations of the design high water level and the top of dam were determined by routing the emergency spillway and freeboard hydrographs developed by the SCS through the reservoir. Both hydrographs were based on a storm duration of 6 hours. A summary of rainfall, hydrograph, and routing data used by the SCS is presented in Appendix D.

- b. Experience Data Washington County personnel reported that the emergency spillway has never been activated on this dam. The maximum pool level of record is approximately at Elevation 905.4 feet M.S.L., 15.5 feet below the crest of the emergency spillway. This level was reached sometime in the summer of 1978 when local residents blocked the intakes on the riser unit. Washington County personnel did not become aware of this situation until the pool level had reached the elevation stated above, at which time the blockage was removed and the reservoir level lowered. No problems were reported to have arisen from this high pool level.
- c. <u>Visual Observations</u> No conditions were observed during the visual inspection which would indicate that the dam and appurtenances could not perform satisfactory during a flood event.
- d. Overtopping Potential PA 485 is an "Intermediate" size "High" hazard dam requiring evaluation for a spillway design flood (SDF) equal to the Probable Maximum Flood (PMF). Since the dam was designed by the SCS using precipitation values approximately equal to the Probable Maximum Precipitation, the dam should be capable of safely passing the SDF without overtopping. After reviewing the

hydrologic and hydraulic calculations prepared by the SCS and judging them to be accurate, it was determined that further hydrologic or hydraulic analyses were unnecessary.

e. <u>Spillway Adequacy</u> - The dam and appurtenances, as outlined above, were designed to safely pass a freeboard hydrograph approximately equal to the PMF. Therefore, the spillway is considered to be "adequate".

SECTION 6 - STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

- a. Visual Observation No structural inadequacies were noted during the visual inspection of PA 485. The small slide in the left abutment upstream from the emergency spillway does not affect the embankment at this time. This area should be monitored in future inspections to ensure that it does not develop into a significant problem.
- b. Design and Construction Data Calculations of embankment slope and foundation stability were not available for review. However, summary reports from the SCS Soil Mechanics Laboratory at Lincoln, Nebraska dated 13 November 1974, 13 June 1972, 21 March 1972, and 23 September 1971 presented the results of the laboratory soil testing program and slope stability analysis performed. Total stress shear strength parameters obtained and used in the slope stability analysis were reported as follows:

Foundation Materials -

Soil Type - Sandy Clay (CL) and Clayey Gravel (GC)
Type of Test Performed - Direct Shear Test

Angle of Internal Friction (0) - 30.5°

Cohesion (c) - 0

Sample Type - Remolded*

*(Note: A Shelby tube sample was obtained for testing; however, because of the gravel, a small diameter undisturbed test sample could not be adequately trimmed. Remolded and compacted samples were then prepared for testing.)

Zone I (core) Embankment Materials -

Soil Type
Silts and Clays (ML, MH, CL)

Type of Test Performed
Consolidated Undrained Triaxial Shear Test

Angle of Internal

Friction (\$\mathcal{\beta}\$)
Cohesion (c)
Sample Type
Silts and Clays (ML, MH, CL)

Consolidated Undrained Triaxial Shear Test

15.5°

Minus No. 4 Sieve, Remolded and Compacted at

100% Standard Proctor

Zone II (shell) Embankment Materials -

Soil Type -

Type of Test Performed -

Angle of Internal Friction (0) -Cohesion (c) -Sample Type - Weathered Siltstone (GM)
Consolidated Undrained
Triaxial Shear Test

15.5°
750 p.s.f.
Mixture of 40% minus
No. 4 material and 60%
rock, compacted to 85%
of Standard Proctor*

*(Note: A method specification was used for construction of the shell material - "minimum 6 passes with a 450 p.s.i. tamping roller per lift.")

Zone III embankment material shear strength is the same as zone II material. Additional testing of the strip mine spoil placed on the borrow area showed the shear strength exceeded the strength parameters presented above.

The results of the stability calculations (using a Modified Swedish Circle Method) for various embankment designs was presented. The resulting minimum factor of safety for the upstream slope under full drawdown conditions and the "as built" configuration was 1.35. The resulting minimum factor of safety for the downstream slope under steady state seepage was 1.52. Design revisions of the drainage system, including a chimney drain, foundation drains, and abutment drainage, would increase the analyzed factor of safety from the reported 1.52.

Based upon the above information, coupled with the visual inspection, it is concluded that further stability assessments of the embankment are not necessary.

- c. Operating Records Nothing in the available operating information indicates cause for concern relative to the structural stability of the dam.
- d. <u>Post-Construction Changes</u> No changes adversely affecting the structural stability of the dam have been performed.
- e. <u>Seismic Stability</u> The dam is located in Seismic Zone I of the "Seismic Zone Map of the Contiguous United States," Figure 1, page D-30, "Recommended

Guidelines for Safety Inspections of Dams." This is a zone of minor seismic activity. Therefore, further consideration of the seismic stability is not warranted.

7.1 DAM ASSESSEMENT

- a. Safety The dam and its appurtenant structures were found to be in good overall condition at the time of the inspection. PA 485 is an "Intermediate" size "High" hazard dam requiring evaluation for an SDF equal to the PMF. As discussed in Section 5, the dam was designed by the SCS to safely pass the PMF without overtopping the dam. The spillway is therefore considered to be "adequate".
- b. Adequacy of Information The information available and the observations made during the field inspection are considered to be adequate for a Phase I Inspection of this dam.
- c. <u>Urgency</u> At the present time, there are no major problems which require remedial action by the owners of the dam.
- d. Necessity for Additional Data/Evaluation No conditions were observed during the inspection of this dam which warrant additional evaluation at this time.

7.2 RECOMMENDATIONS/REMEDIAL MEASURES

The inspection and review of information revealed several minor deficiencies which require remedial measures by the owners of the dam.

- Remove the debris which has collected in the trash rack in front of the low-level intake on the riser unit.
- 2) Repair the minor tire rutting along the crest of the dam. Vehicles should be prevented from traveling along the dam crest.
- 3) Reseed the areas along the dam crest and berm on the upstream face of the embankment where vegetation is sparse.
- 4) Repair the erosion gully on the downstream side of the dam along the junction of the embankment and right abutment.

5) Regrade the berms on the downstream face of the embankment to provide better surface drainage.

It is also recommended that the slide in the left abutment immediately upstream from the emergency spillway be monitored during future inspections to ensure that this does not become a significant problem.

In addition, the following operational measures are recommended to be undertaken by the owner:

- 1) Develop a detailed emergency operation and warning system.
- 2) During periods of unusually heavy rainfall, provide around-the-clock surveillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, the owner should activate the emergency operation and warning system.

APPENDIX A

VISUAL INSPECTION CHECK LIST, FIELD SKETCH, TOP OF DAM PROFILE, AND TYPICAL CROSS-SECTION

Phase 1 Vigual Inspection Check List

PA Coordinates Lat. N 40°22.2'	Cloudy, cool Temperature 50° F.	railwater at Time of Inspection ft.* M.S.L. the northwest corner of the impact basin, by the SCS).	Owner's Representatives:		PennDER:	William Francis
Name of Dam PA 485 County Washington State	NDI # PA 01123 PennDER # 63-81 SCS # PA 485 Date of Inspection 20 March 1980 Weather	Pool Elevation at Time of Inspection ft.* M.S.L. Tailwater at Time of Inspection ft.* *All elevations are referenced to a bench mark on the northwest corner of the impact basin, El. 860.4 ft. M.S.L. (bench mark was established by the SCS).	Inspection Personnel: Michael Baker, Jr., Inc.:	Jeffrey A. Quay Larry A. Diday George A. Slagle	Field Review (9 June 1980):	John A. Dziubek James G. Ulinski

Recorder

Jeffrey A. Quay

CONCRETE/MASONRY DAMS - Not Applicable

		REMARKS OR RECOMMENDATIONS
		OBSERVATIONS
Name of Dam: PA 485	NDI # PA 01123	VISUAL EXAMINATION OF

LEAKAGE

STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS

DRAINS

WATER PASSAGES

FOUNDATION

CONCRETE/MASONRY DAMS - Not Applicable

Name of Dam: PA 485 NDI # PA 01123 VISUAL EXAMINATION OF OBSERVATIONS	
SURFACE CRACKS CONCRETE SURFACES	
STRUCTURAL CRACKING	
VERTICAL AND HORIZONTAL ALIGNMENT	
MONOLITH JOINTS	
CONSTRUCTION JOINTS	

REMARKS OR RECOMMENDATIONS

EMBANKMENT

Name of Dam PA 485

NDI # PA 01123

VISUAL EXAMINATION OF

SURFACE CRACKS

None observed

OBSERVATIONS

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE

None observed

SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES

There is a small slide above the left abutment immediately upstream from the emergency spillway. Earth has slid into the reservoir.

(Note: A small mud slide was observed during the field review on the downstream left abutment immediately above the rock gutter 30 ft. from the crest. This soil may clog the rock gutter.) There is a small erosion gully on the downstream side of the dam along the junction of the embankment and right abutment.

The slide does not block the emergency spillway or affect the embankment. It does not represent a significant problem at the present time. The erosion gully should be repaired.

EMBANKMENT

PA 485 Name of Dam

NDI # PA 01123

VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST VISUAL EXAMINATION OF

appeared to be good. There are vehicle tracks and some minor tire rutting on The vertical and horizontal alignment the crest.

OBSERVATIONS

Vehicles should be prevented from driving on the crest of the dam.

REMARKS OR RECOMMENDATIONS

RIPRAP FAILURES

itself. Riprap placed along the abutment/embankment contacts and below the impact basin is in good condition. No riprap has been used on the embankment

VEGETATION

tion is also sparse on the berm on the upstream side of the embankment. crest and in small scattered locations on the downstream embankment. Vegeta-The embankment is covered with crown vetch. Vegetation is sparse on the

Areas in which the vegetation is sparse should be reseeded.

EMBANKMENT

Regrade the berms on the downstream face to provide better surface drainage. REMARKS OR RECOMMENDATIONS The berms on the downstream face have these areas are above the normal pool elevaa small amount of standing water which probably collected as a result of recent precip-None was observed. The downstream embankment is wet where vegetation is sparse, but OBSERVATIONS No problems observed itation. tion. None STAFF GAGE AND RECORDER JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM ANY NOTICEABLE SEEPAGE VISUAL EXAMINATION OF NDI # PA 01123 Name of Dam

None observed

DRAINS

OUTLET WORKS - Principal Spillway

PA 485

Name of Dam:

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	The conduit could not be observed.	·
INTAKE STRUCTURE	The intake structure is a standard SCS two-stage riser. Concrete is in good condition. Some trash has accumulated around the trash rack at the low-level orifice.	The trash rack should be cleaned.
OUTLET STRUCTURE	'ine outlet structure is a concrete impact basin. Concrete is in good condition.	
OUTLET CHANNEL	The outlet channel is riprapped for the first 15 ft. Water in the outlet channel is high as a result of backwater from obstructions in the downstream channel. These obstructions are described on Page A-12.	The backwater in the outlet channel does not significantly restrict flow from the principal spillway.
EMERGENCY GATE	The inlet to the reservoir drain is located at the base of the riser unit on the upstream side. The inlet is controlled by a 30 in. slide gate operated by controls on the top of the riser unit.	

UNGATED SPILLWAY - Emergency Spillway

PA 485

Name of Dam:

NDI # PA 01123 VISUAL EXAMINATION OF	OF OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONTROL SECTION	The control section for the emergency spillway is a 30 ft. wide (parallel to the direction of flow) by 50 ft. long (perpendicular to the direction of flow) level section. No problems in this section were observed.	
APPROACH CHANNEL	The emergency spillway channel consists of a vegetated earth and rock cut in the hillside next to left abutment. The channel was in good condition. Some water has collected in the emergency spillway.	The water present is probably the result of recent precipi- tation.
DISCHARGE CHANNEL	The discharge channel has the same configura- tion as the approach channel; no problems were observed.	
BRIDGE AND PIERS	None	

GATED SPILLWAY - Not Applicable

PA 485

Name of Dam: NDI # PA 01123

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SILL		
APPROACH CHANNEL		
DISCHARGE CHANNEL		
BRIDGE AND PIERS		

GATES AND OPERATION EQUIPMENT

INSTRUMENTATION

NDI # PA 01123 Name of Dam:

PA 485

VISUAL EXAMINATION

MONUMENTATION/SURVEYS

Seventeen (17) crest monuments were installed along the centerline of the dam crest to monitor the settlement and alignment of the dam.

OBSERVATIONS

REMARKS OR RECOMMENDATIONS

OBSERVATION WELLS

None

WEIRS

None

PIEZOMETERS

Twelve (12) piezometers were installed at various locations on the dam; 3 along the centerline of the dam crest, 5 in the downstream embankment and foundation, and

4 along the downstream toe of the embank-ment in the insitu soil.

OTHER

RESERVOIR

PA 485 Name of Dam:

NDI # PA 01123

REMARKS OR RECOMMENDATIONS problem. spillway). A small slide has occurred and erosion gullies are forming in this area. Slopes are steep and wooded. The only area where erosion is occurring is on the left (east) slope at the downstream end of the reservoir (immediately upstream from the entrance to the emergency OBSERVATIONS VISUAL EXAMINATION OF SLOPES

future inspections to ensure that it does not develop into a major area should be monitored during The slide is not a significant problem at this time. This

SEDIMENTATION

represent a significant reduction in available sedia faster rate than that anticipated by the SCS. The slide into the reservoir mentioned earlier does not was no evidence that sedimentation was occurring at The dam was designed with a sediment storage volume equal to a 50-year accumulation of sediment. There ment storage.

DOWNSTREAM CHANNEL

Name of Dam:

PA 485

NDI # PA 01123

OBSERVATIONS VISUAL EXAMINATION OF

REMARKS OR RECOMMENDATIONS

(OBSTRUCTIONS, CONDITION

DEBRIS, ETC.)

ft. downstream from the impact basin. A fence A 1.0 ft. high board has been placed across the bottom of the outlet channel approximately 150

to back up water in the channel, forming a pool approximately 2 ft. deep. This was apparently collecting in the fence and the board combine

done to provide an area for geese. This does not represent a serious obstruction to flow out

of the outlet channel.

Slope of the channel is moderate.

SLOPES

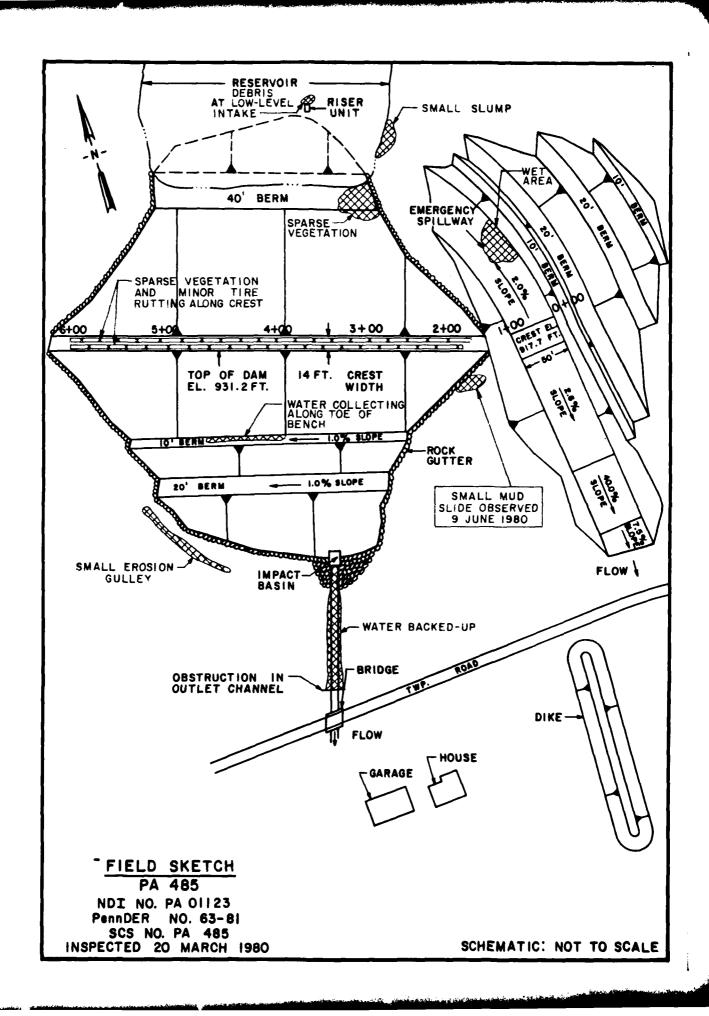
APPROXIMATE NO. OF HOMES AND

POPULATION

Harmon Creek, the closest of which is approx-Two houses are located between the dam and imately 200 ft. downstream from the dam.

Township route T-819 is also located approx-

imately 175 ft. downstream from the dam.



MICHAEL BAKER, JR., INC.

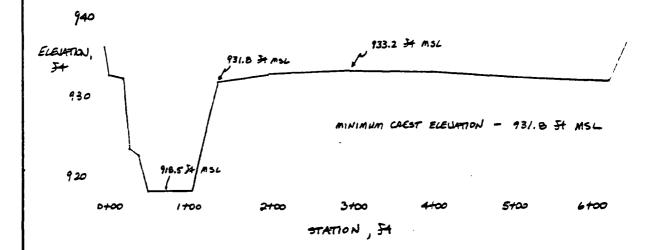
THE BAKER ENGINEERS
14 May 1980
Box 280
Beaver, Pa. 15009

PA 485

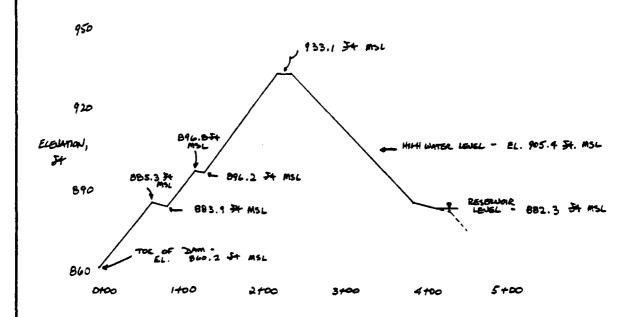
TOP OF DAM PROFILE TYPICAL CROSS-SECTION

DATE OF INSPECTION - 20 March 1980

TOP OF DAM PROFILE



cross-section at 5th 3+12



APPENDIX B

ENGINEERING DATA CHECK LIST

ENGINEERING DATA CHECK LIST SN. CONSTRUCTION. OPERATION

Name of Dam: PA 485 NDI # PA 01123

CHECK LIST
DESIGN, CONSTRUCTION, OPERATION

ITEM

PLAN OF DAM

See Plate 3.

REGIONAL VICINITY MAP

The Avella, Burgettstown, and Steubenville East, PA and Weirton, WV - PA - OH 7.5 minute USGS topographic quadrangles were used to prepare the regional vicinity and watershed maps included as plates 1 and 2 in this report.

CONSTRUCTION HISTORY

Construction of the dam began in April 1976 and was completed in October 1977. The contractor responsible for construction was October 1977. The contractor respons. Solomon - Teslovich of Masontown, PA.

TYPICAL SECTIONS OF DAM

See Plates 5 and 10 and Appendix A, Sheet 14.

HYDROLOGIC/HYDRAULIC DATA

Design computations from the SCS design report for PA 485 were reviewed for this report. These calculations are summarized in Sections 5 and Appendix D.

OUTLETS - PLAN

See Plate 11.

- DETAILS

See Plates 12, 13, and 14.

- DISCHARGE RATINGS

CONSTRAINTS

Discharge ratings were included in the SCS design report for this dam and are summarized in Appendix D.

RAINFALL/RESERVOIR RECORDS

None available

PA 485 Name of Dam:

NDI # PA 01123

ITEH

REMARKS

DESIGN REPORTS

The SCS design report for PA 485 is available from the Harrisburg, PA SCS office.

GEOLOGY REPORTS

See Appendix F for the regional geology; additional information is available in the SCS design report for PA 485.

HYDROLOGY & HYDRAULICS DESIGN COMPUTATIONS DAM STABILITY

SEEPAGE STUDIES

These analyses are all contained in the SCS design report for PA 485.

MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD

The results of foundation and borrow excavation tests are contained in the SCS design report for this dam.

POST-CONSTRUCTION BURVEYS OF DAM

None

BORROW SOURCES

Some material was also taken from the valley floor upstream from the dam and from the emergency spillway excavation. Further specifications concerning the borrow material used are contained in the The majority of the borrow material used for construction of the embankment was taken from the area above the left abutment. SCS. design report.

Name of Dam:

17 crest monuments and 12 piezometers were installed at the dam site. Their locations are shown in Plates 15 and 7, respectively. REMARKS None MONITORING SYSTEMS MODIFICATIONS ITEM

This No problems were reported as a result of this by Washington County personnel until water had reached the elevainlets on the riser unit. This was not discovered and corrected high water resulted when local residents reportedly blocked the The highest pool level of record is at El. 905.4 ft. M.S.L. tion stated above. high water level. None POST-CONSTRUCTION ENGINEERING STUDIES AND REPORTS HIGH POOL RECORDS

PRIOR ACCIDENTS OR FAILURE OF DAM None DESCRIPTION REPORTS

No records are available. Routine maintenance is performed by Washington County personnel.

MAINTENANCE OPERATION RECORDS

PA 485 Name of Dam:

NDI # PA 01123

REMARKS

ITEM

SPILLWAY PLAN,

SECTIONS, and

See Plates 3 and 4. DETAILS

OPERATING EQUIPMENT PLANS & DETAILS

The only operating equipment is the 30 in. gate valve controlling the reservoir drain. The location of this drain is shown on Plates 11 and 13.

CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

DRAINAGE A	AREA CHARACTERISTICS: 2.18 sq.mi. (Primarily forested with
	some residential areas in the upper portion of the basin)
ELEVATION	TOP NORMAL POOL (STORAGE CAPACITY): 879.5 ft. M.S.L.
	(43.5 acft.)
ELEVATION	TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 917.7 ft. M.S.L.
	(536.8 acft.)
ELEVATION	MAXIMUM DESIGN POOL: 920.9 ft. M.S.L. (621.8 acft.)
ELEVATION	TOP DAM: 931.8 ft. M.S.L. (minimum top of dam)
SPILLWAY:	Emergency Spillway
a. b. c.	Crest Elevation 917.7 ft. M.S.L. Type Vegetated trapezoidal earth and rock cur channel Bottom Width (Perpendicular to Flow) 50 ft.
đ.	Length of Spillway along Centerline (Parallel to Flow)
e. f.	Location Spillover Left abutment Number and Type of Gates None
OUTLET WO	RKS: Principal Spillway
a.	Type 2-stage drop-inlet riser connected to a 30 in. concrete
b.	Location 250 ft. from the left abutment outlet pipe
c.	Entrance Inverts El. 879.5 ft. M.S.L. (low-level inlet); Exit Inverts El. 853.0 ft. M.S.L. El. 895.5 ft. M.S.L.
đ.	Exit Inverts El. 853.0 ft. M.S.L. El. 895.5 ft. M.S.L.
	(upper-level inlet)
e.	Emergency Drawdown Facilities 30 in. drain, invert El.
HYDROMETE	DROLOGICAL GAGES: None 855.5 ft. M.S.L. at base of riser unit.
a.	Type
b.	Location
c.	Records
MAXIMUM KI	NOWN NON-DAMAGING DISCHARGE 120 c.f.s.

APPENDIX C

PHOTOGRAPH LOCATION PLAN AND PHOTOGRAPHS

DETAILED PHOTOGRAPH DESCRIPTION

Overall View of Dam

Top Photo - Overall View of Upstream Face of Dam from

(OV-T) Reservoir Area

Bottom Photo - Overall View of Crest of Dam and Downstream

(OV-B) Face from Right Abutment

Photograph Location Plan

Photo 1 - View along Crest of Dam from Right Abutment

Photo 2 - View of Riser Unit from Reservoir Area

Photo 3 - View of Debris on Upstream Face of Dam
(Note: debris was deposited by high water level described in Section 5)

Photo 4 - View of Eroded and Sloughing Area of Reservoir Slope to the Left of Emergency Spillway

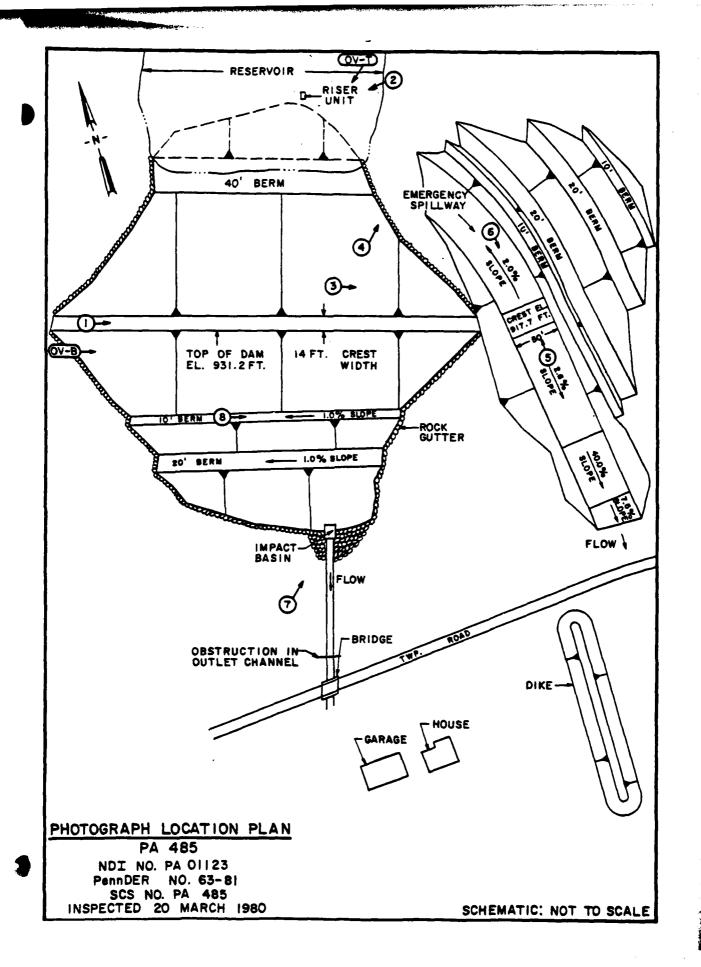
Photo 5 - View of Emergency Spillway Looking Upstream

Photo 6 - View of Emergency Spillway Looking Downstream

Photo 7 - View of Impact Basin and Rock Gutter along Left
Abutment

Photo 8 - View of Water Collecting at Toe of Bench on Downstream Side of Embankment

Note: Photographs were taken on 20 March 1980.



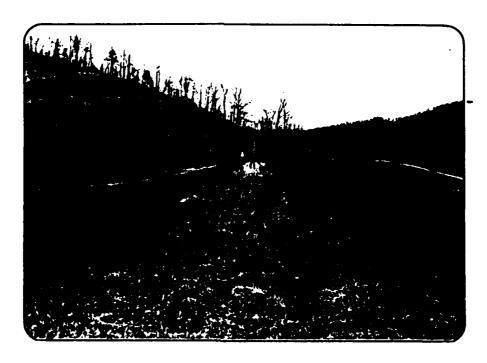


PHOTO 1. View along Crest of Dam from Right Abutment

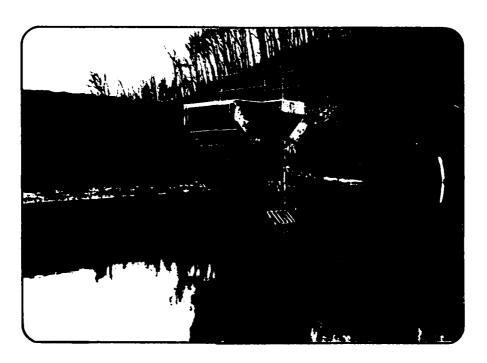


PHOTO 2. View of Riser Unit from Reservoir Area



PHOTO 3. View of Debris on Upstream Face of Dam

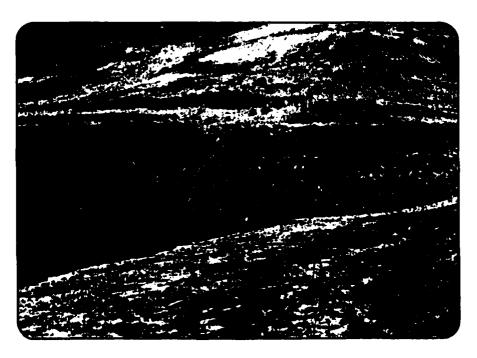


PHOTO 4. View of Eroded and Sloughing Area of Reservoir Slope to the Left of Emergency Spillway

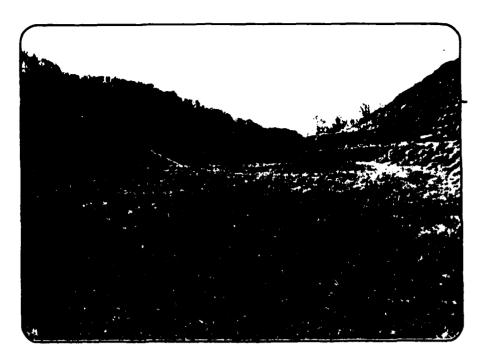


PHOTO 5. View of Emergency Spillway Looking Upstream



PHOTO 6. View of Emergency Spillway Looking Downstream



PHOTO 7. View of Impact Basin and Rock Gutter along Left Abutment



PHOTO 8. View of Water Collecting at Toe of Bench on Downstream Side of Embankment

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

MICHAEL BAKER, JR., INC.	Subject PA 485	_ S.O. No
THE BAKER ENGINEERS	APPENDIX D - HYDROLOGIC AND	
Box 280	H40 P2446 - 22 - 15	_ Drawing No
Beaver, Pa. 15009	Computed by Checked by	- Date

<u>Jubject</u>	TAKE
HYDROLOGY AND HYDRAULIC DATA	
BASE	1
REMARKS	2
HYDROLOGIC DATA	3
STACE US. AREA, STOTEAUE, DISCHARGE DATA	4
TOP OF DAM PROFILE AND	
TYPIAL CROSS · SECTION	چ
DRAMAGE BASIN MAP	6

HYDROLOGY AND HYDRAULIC ANALYSIS DATA BASE

NAME OF DAM: PA 485						
PROBABLE MAXIMUM PRECIPITATION (PMP) = 24.1 INCHES/24 HOURS (1)						
STATION	1	2	3	4	5	
Station Description	PA 485					
Drainage Area (square miles)	2.18					
Cumulative brainage Area (square miles)	2.18					
Adjustment of PMF (for Drainage Area (%)	Zone 7					
6 Hours 12 Hours 24 Hours 48 Hours 72 Hours	102 120 130 140					
Snyder Hydrograph Parameters						
Zone (3)	28B					
c _p /c _t (4)	0.57/1.7					
L (miles) (5)	2.89					
L _{ca} (miles) (5)	1.53					
$t_p = C_t (L \cdot L_{ca})^{0.3} \text{ (hours)}$	2.66					
Spillway Data Crest Length (ft) Freeboard (ft) Discharge Coefficient Exponent	(Spillway rating o	curve information	is presented on S	heet 4)		
(1) Hydrometeorological Report (2) Hydrometeorological Report						

 $^{^{(3)}}$ Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snyder's Coefficients $^{(C_p)}$ and $^{(C_p)}$.

⁽⁴⁾ Snyder's Coefficients.

 $^{^{(5)}}L$ = Length of longest water course from outlet to basin divide. L_{ca} = Length of water course from outlet to point opposite the centroid of drainage area.

N	fichael Baker, Jr., Inc.
1	THE BAKER ENGINEERS

Box 280 Beaver, Pa. 15009

Subject	PA 485		S.O. No
			Sheet No. 2 of 6
			Drawing No
Commissed by	WDL	Charled by	5/29/80

PA 485 was designed by the SCS in accordance with standard oriteria for structures of this type. He design fleod used by the SCS for this dam is based on precipitation essentially equal to the Probable maximum Precipitation. Merefore, the dam should be capable of passing the Probable maximum Hood (PMF) without overtapping.

a summary of the key information used by the 5CS in the design of PA 485 is included on the following pages.

MICHAEL	BAKER,	JR.,	INC.

THE BAKER ENGINEERS

Box 280 Beaver, Pa. 15009 Computed by UDL Checked by _____ Date 5-3/-80

THE FOLLOWING ENFORMATION WAS TAKEN FROM THE SCS DESIGN REFRONT:

DRAINAGE AREA = 2.18 59, MI.

TIME OF CONCENTRATION = 1.39 HOURS

CURUE NUMBER (AMC II) = 74

STORM DURATION = 6 HOURS

HOROCRAPH	RAINFALL (ZN)	Runoff (IN)	THEOW (cfs)	PEAK antion (cfs)	maximum zesepudr surface eced.(ft)
emercency Spillway	9. 4 5	6.25	3,304	B25	920.9
FREE BOARD	25.5	21.7	11,800	8,693	931.2

6 HOUR PAP (From HMR-33) = 24.6 ENCHES

	MICHA	EL	BAKER,	JR	INC.
--	-------	----	--------	----	------

THE BAKER ENGINEERS

Box 280 Beaver, Pa. 15009

Subject PA 485	S.O. No
STACE US. AREA STORAGE DATA	Sheet No. 4 of 6
STAGE US. DISCHARGE DATA	
6	_

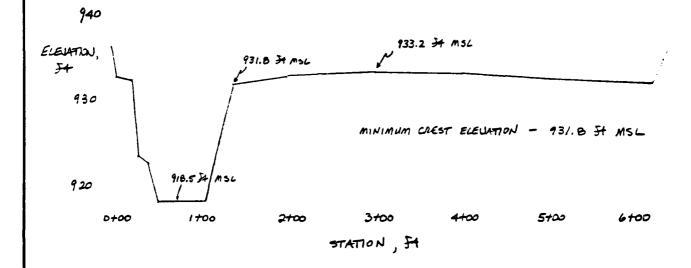
THE FOLLOWING DATA WAS TAILEN FROM THE SCS DESIGN REPORT FOR PA 485:

STAGE (FL)	AREA (Ac.)	5TORALE (AL-\$4)	REAGRES
879.5	5.7	43.5	INUST OF BRIFICE
<i>885.0</i>	7.7	83	
890.0	9.9	127	
895.5	12.4	189.8	CREST OF TLISER (LIPPER LEVEL ZUTAKE)
910.0	19.9	418	111-11-12
917.7	25.5	536.B	CREST OF EMBRICANCY SPILLING
920.9	<i>₽7.</i> 7	621.8	DESIGN HILH WHER
925.0	31.4	800	
931.2	37	951.8	TOP OF DAM

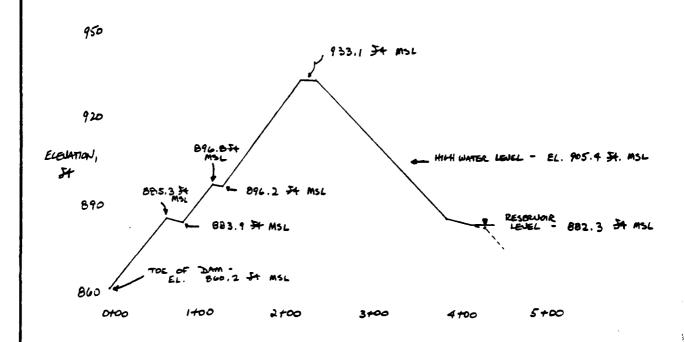
3TAUE (54)	DISCHARLE (C+S)	REMARKS
879.5	0	INST OF DUFICE
880,0	1.65	
882.0	10.2	
885.0	16.2	
891.0	24.0	
6 13 .0	26.1	
895.5	28.5	crest of puser (upper level thinks)
897.0	115	,
117.7	132	LIEST OF GMERCENCY SPILLINGLY
920,9	825	DESIM HILL WATER
931.2	8693	TOP OF DAM

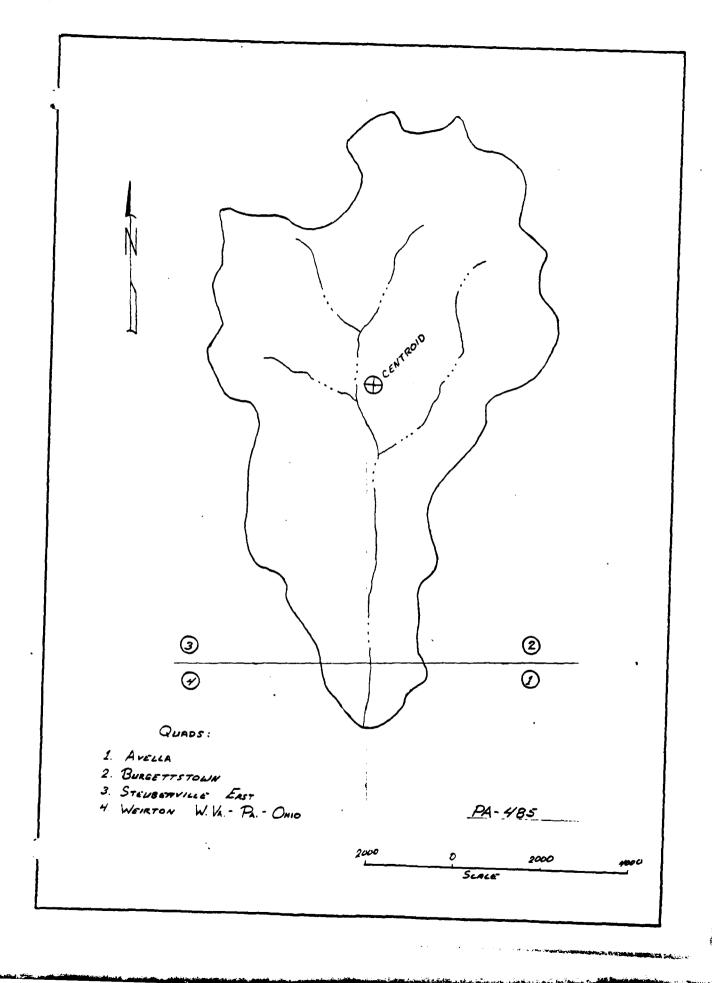
MICHAEL BAKER, JR., INC.	Subject	TOP OF DAM	PROFILE A	4	S.O. Ne	· ·
THE BAKER ENGINEERS	TYPICAL CROSS-SECTION			Sheet N	10. <u>5</u> of <u>6</u>	
5		_			Drawing	No
Box 280	Computed by	LAS	Checked by	WDL	Data	5-14-80

TOP OF DAM PROFILE



CROSS-SECTION AT STA 3+12



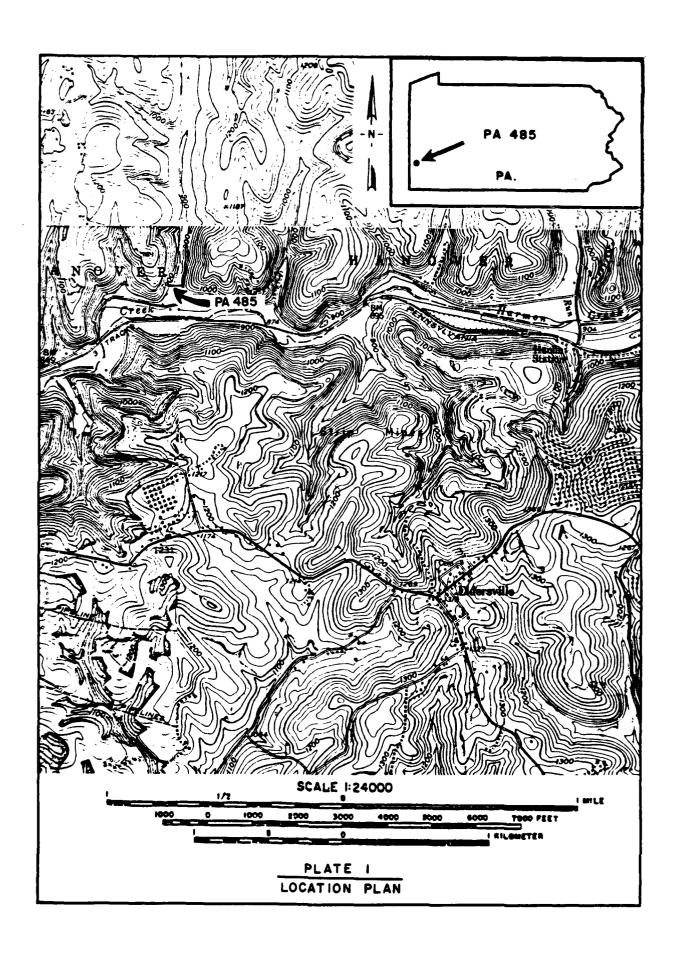


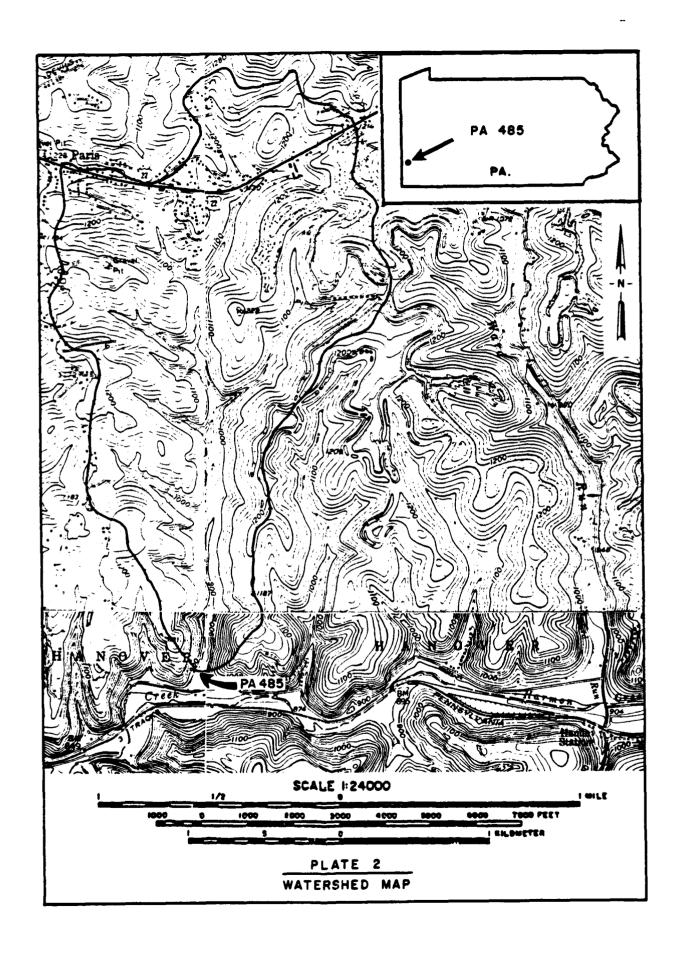
APPENDIX E

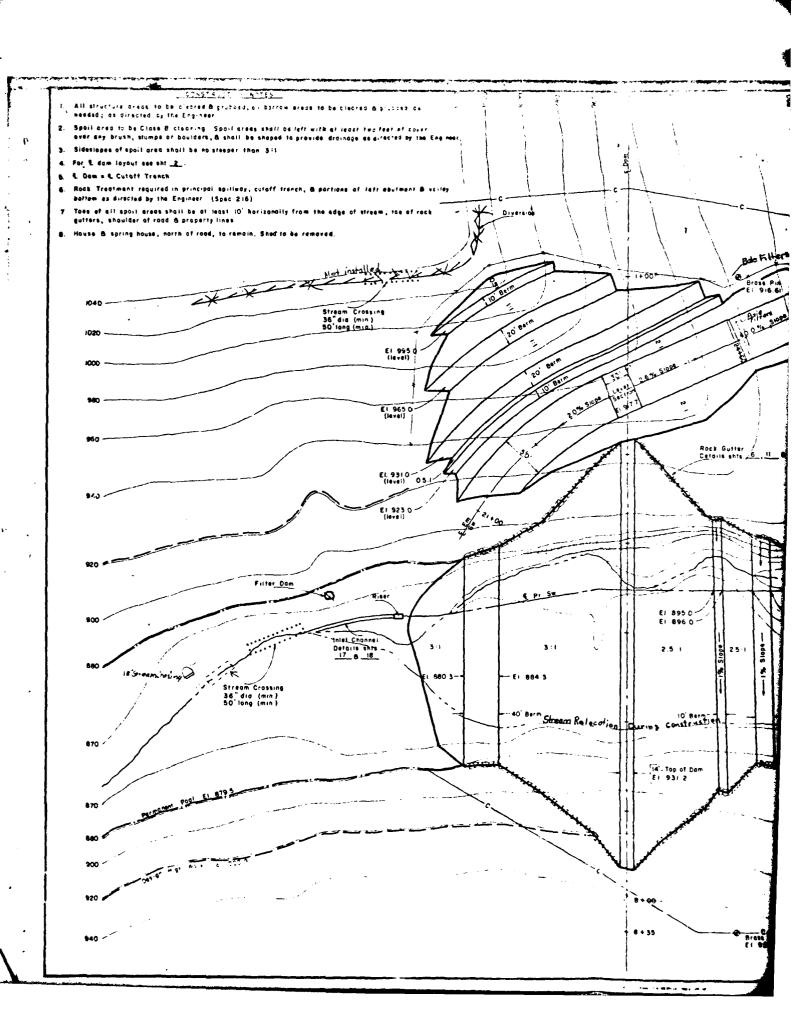
PLATES

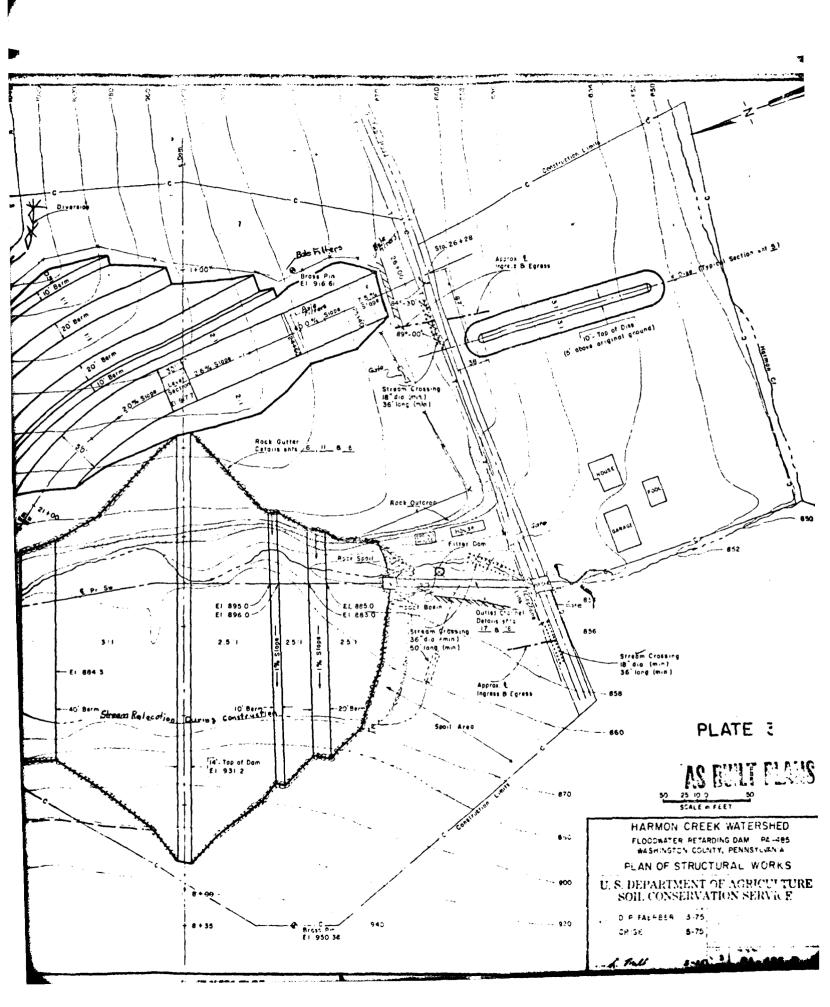
CONTENTS

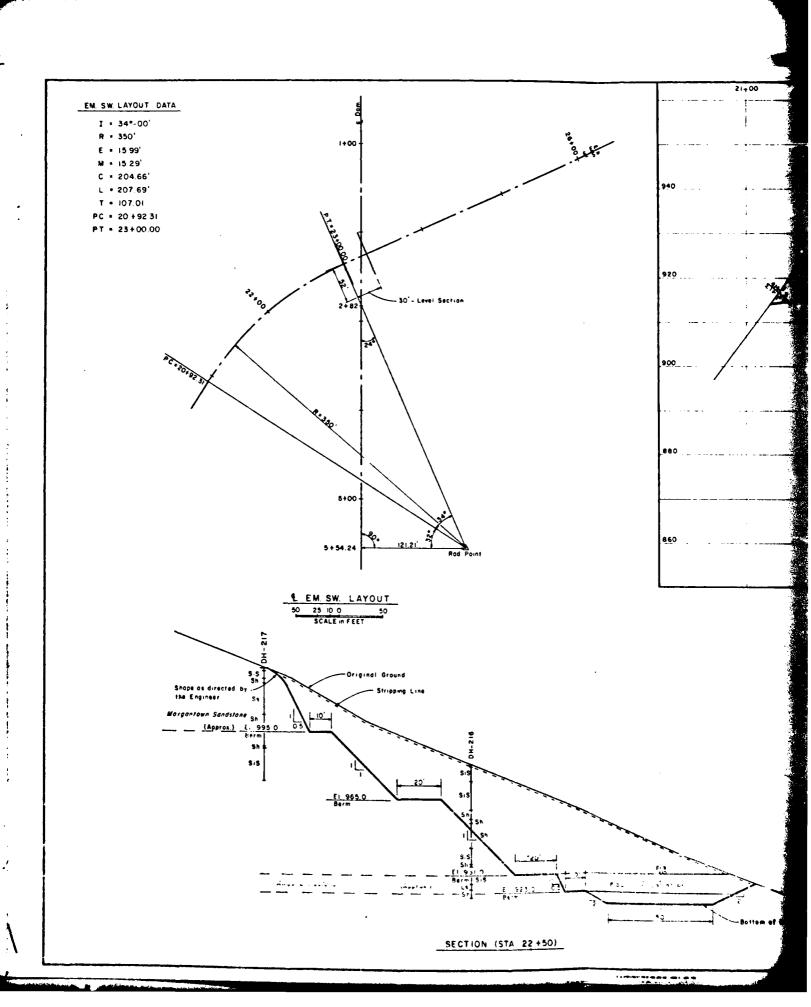
- Plate 1 Location Plan
- Plate 2 Watershed Map
- Plate 3 Plan of Structural Works
- Plate 4 Emergency Spillway
- Plate 5 Fill Placement
- Plate 6 Cut-off Trench
- Plate 7 Piezometer Installation
- Plate 8 Foundation Drainage
- Plate 9 Chimney Drain
- Plate 10 Chimney Drain (Sections)
- Plate 11 Principal Spillway
- Plate 12 Principal Spillway (Profile)
- Plate 13 Riser
- Plate 14 Impact Basin
- Plate 15 Crest Monument Installation

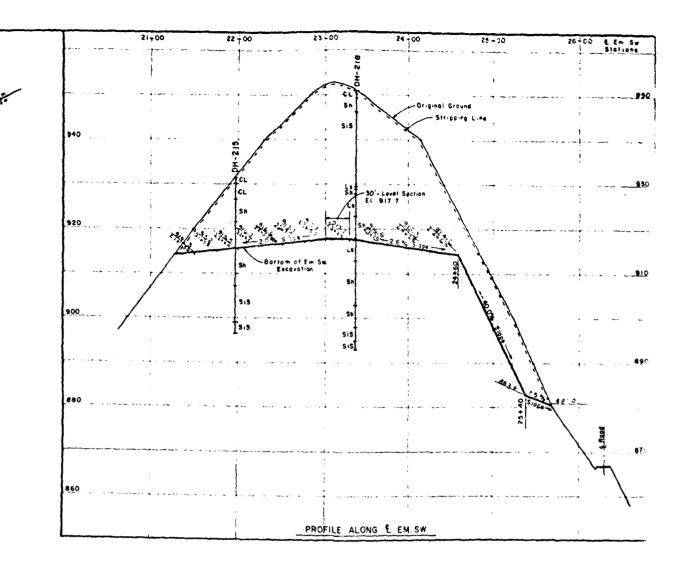












NOTE -

Engineer may authorize changes to sideslapes and berms in outside cut to reflect geologic conditions encountered

PLATE 4 AS BUILT FLANS

HARMON CREEK WATERSHED FLOCOWATER RETARDING DAM PA . 195 #45MINGTON COUNTY, PENNSYLVANIA

EMERGENCY SPILLWAY

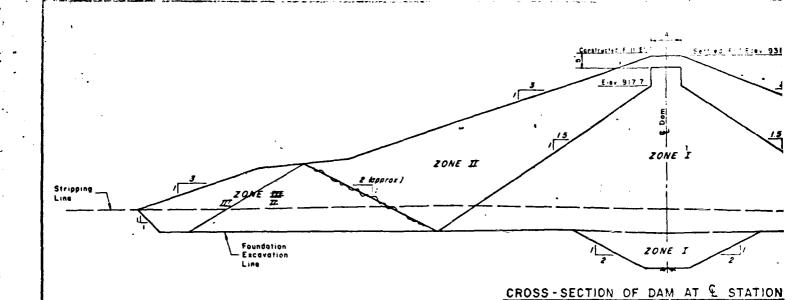
U.S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

DIP PARAGER 3-75.

CRICK 3.75,

2 K.11 4.75 PA-485-P

2+50)



Original Ground

2 one I

Stripping Line

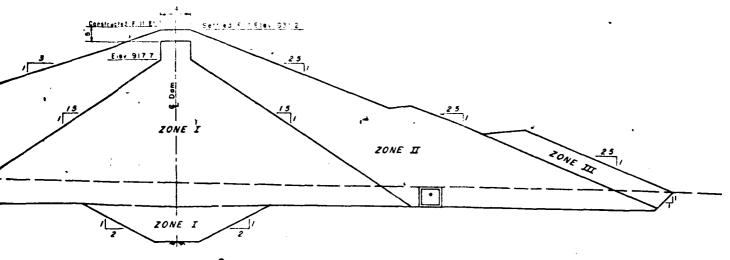
TYPICAL	SECTION OF DIKE	
	NOT TO SCALE	•

SELECTIVE	MATERIAL	MAX &	T WAX T	REO'D E		COMPACTION 3
LACEMENT		SIZE	LIFT	CONTENT	CLASS	SEFINITION
ZONE I	Material as represented by TP-103A, depth 5.5° to 10.0° cit is fed as ML, TP-202A, 10° to 2.3° classified as CU, TP-203A, 10° to 3.0° classified as CU, TP-203A, 3.0° to 6.0° classified as CI, Tourid, thus Escavarion (Alluvium CL and UC)	6.	9"	-2% to +2% of Option: m	A	IOO% Standard density by ASTM 0:600, McCl ad R
20NE II	Materia: 32 represented by TP-1064, depth 3-21 to 6-0', crassif ed as GM, Pesiduals (SM-GP) Mine Spoit	12*	18"	-2% to +2% of Octomum Minus 3/4° mo- terial - ASTM D-698 Me- thad D	С	Minimum 6 passes with a 45C ps i tamping roller per itt

}	SELECTIVE PLACEMENT		MAX AL ROCK S1ZE	의 MAX 의 LIFT	REO'D. WATER CONTEN
	ZONE III	Material from Emergency Spillway, Cutoff Trench, Principal Spillway and let abutment race excavation and cobbles and bounders raked from Zones I & II	-	36'	hature! Moisture

0 5 10 20 30 40 FEET

- Maximum permissible lift thickness before compection
- 2) Water content of full matrix of time of compaction. Ve may be approved by the Engineer
- 크 For typical composition curves see sheets 51 and 51
- 4) For hand consecred backfill, the meximum rock size st not exceed 4.



CROSS-SECTION OF DAM AT & STATION 5+30

o	5	10	20	30	40	FEET
	-	==		-		
			SCALE			



PLATE 5

CONSTRUCTION NOTES

- † For constucted fill elevations see sheet . 7 .
- 2. For berm elevations and slapes see sheet 3

AS BUILT PLANS

HARMON CREEK WATERSHED

FELLILAATER RETARDING DAM PA-485 AASHINSTON COUNTY, PENNSYLVANIA

FILL PLACEMENT

U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

D P FAERBER 3-75 . R. A. STALTER

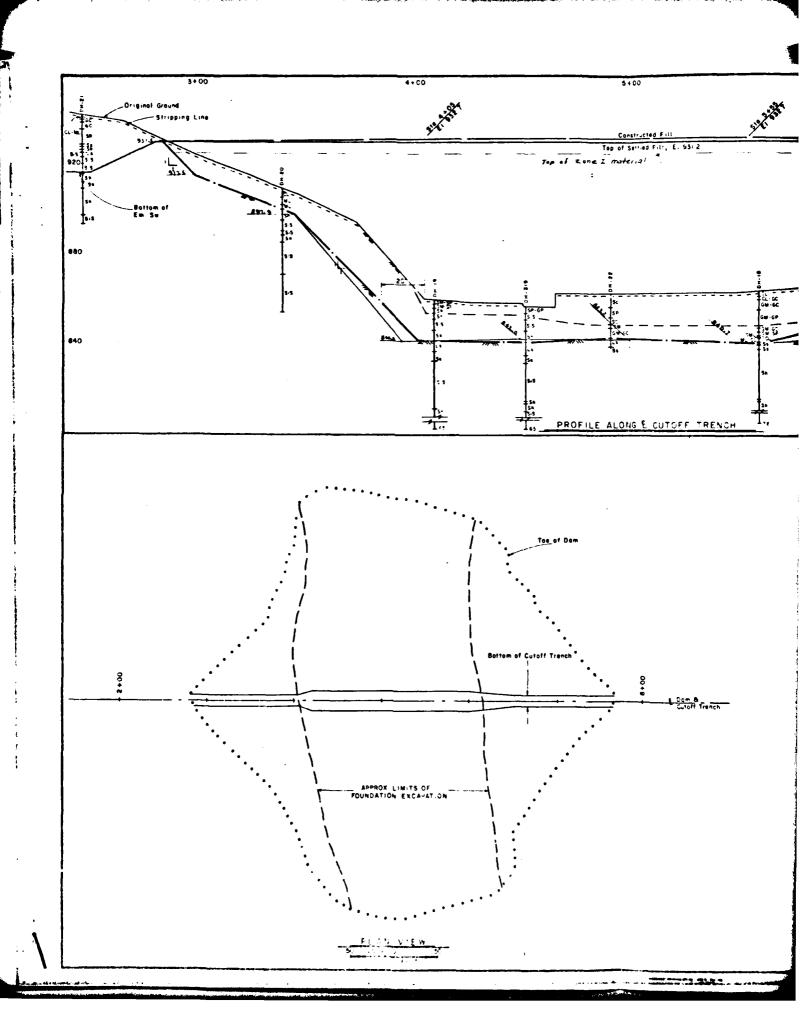
6 - 74

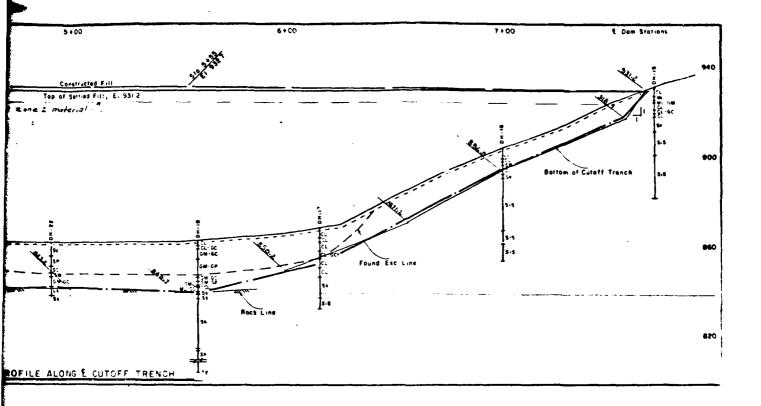
..... CRISE PA-485-P A fieli

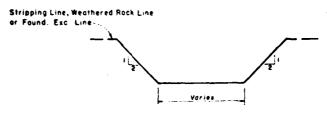
4 S F Sto. 112 B Rev. T. 6

SELECTIVE	I MATERIAL	MAX 4	규 WAX 하	REO'D E		COMPACTION 3
PLACEMENT		SIZE	LIFT	CONTENT	CLASS	DEFINITION
	Material from Emergency Spillway, Cutoff Trench, Principal Spillway and left abutment race excavation and cobbles and boulders	24"	36*	Naturat Moisture	С	Minimum 4 passes per lift with a crawler dozer weigh ing 20 ton or more

- I Maximum permissible lift thickness before compaction
- 2) Water content of fell matrix at time of compaction. Validation from water content shown may be approved by the Engineer
- 2) For typical compatition curves see sheets 51 and 52
- 4) For hand composted backfill, the maximum rock size shall not exceed 3" 8 of thickness shall not exceed 4".







STATION	BOTTOM MIDTH
2+85 to 4+05	12
4+05 to 4+20	Trans tien
4+20 10 6+00	22
6+ 00 to 6+50	Transition
6+ 50 to 7+70	12'

SECTION

CONSTRUCTION NOTES

Cutoff Trench

- 1 & Dom = & Cutoff Trench
- 2 For logs of test holes see shts 37 thru 50
- 3 Rock treatment required in Cutoff Trench bottom as directed by the Engineer.
- 4 The depth of cutoff excavation shown is approximate. The final depth will be determined by the Engineer ofter examination of materials encountered.

PLATE 6

AS BELT PLANS

HARMON CREEK WATERSHED FLOODWATER RETARDING DAM PA 485 WASHINGTON COMMINE, FLANOYLVANIA

CUTOFF TRENCH

et si department of agriculture soil conservation service

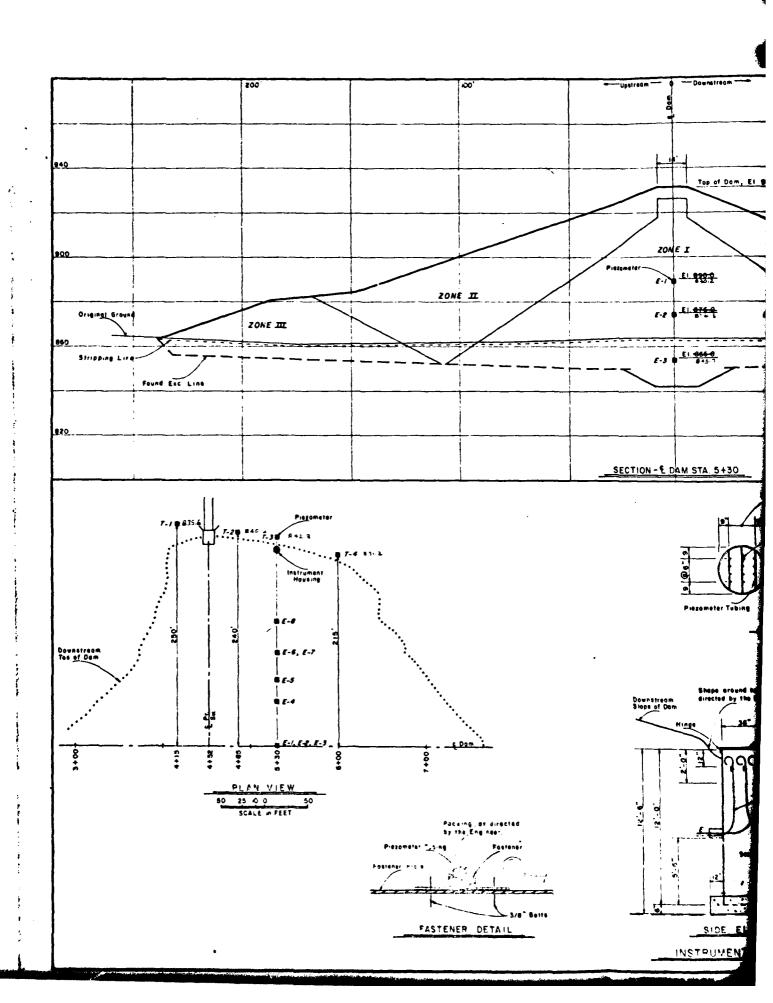
DP FAERBER 3-75

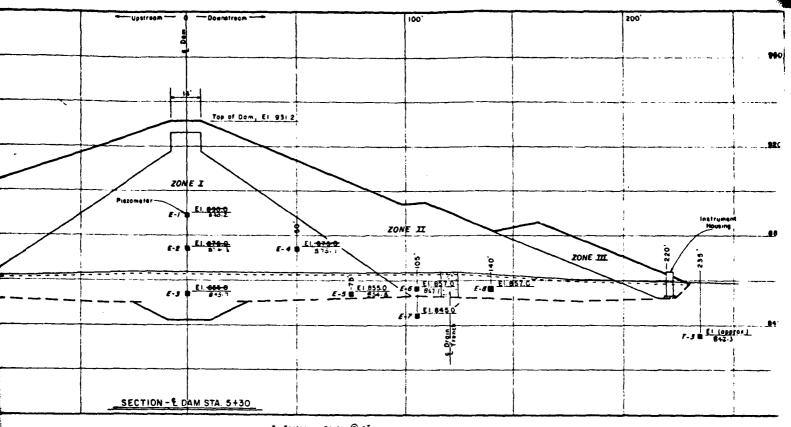
CHISE

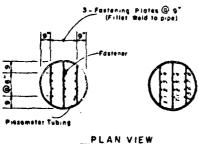
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17:11 4.77 52 PA-485-P

Sta ENG HER Ben.

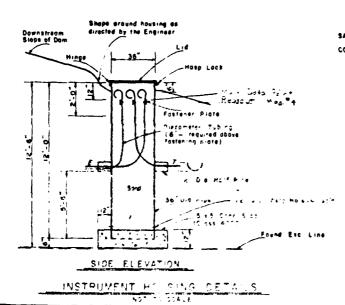






INSTRUMENT HOUSING BILL OF MATERIAL

ITEM	SIZE	LENGTH	QUARTITY
PIPE, Class I, Shape 1, 12 Gage (Spec 551)	36" 010	12'-0"	1
MALF PIPE, Class I, Shape 1, 16 Gage (Spec 551)	12" dis	12"	2
LID. Steel Sheet	/4 36 00		
FASTENER PLATE, GOLV	74 4	VCF:es	3
FASTENER	1/2 die		12
BOLTS, Gaiv., w/ Nuts and Washers	3/8 dia	1"	24
HASP LOCK	1/2" a 4"		
HINGE (As Per Manufacturer Recommendations)		_ - _	•
LOCK (Moster - w/2 keys)			



SAND (Fine Drain Fill - Gredation Limits sht. 11) CONCRETE (Class 4000) 1.0 Cu. Yde.

PLATE 7

AS RELT FLAHS

MARMON CREEK WATERSHED FLOODWATER RETARDING DAM PA-485 WASHINGTON COUNTY, PENNSYLVANIA

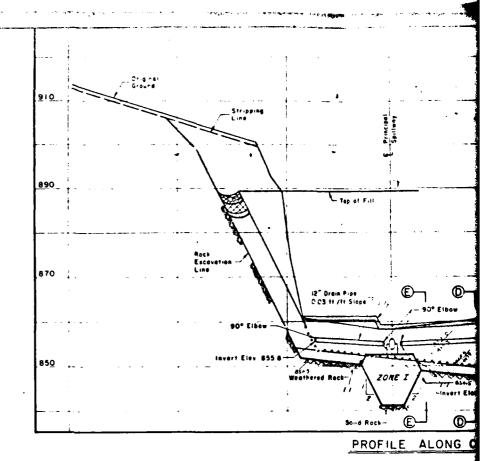
PIETOMETER INSTALLATION

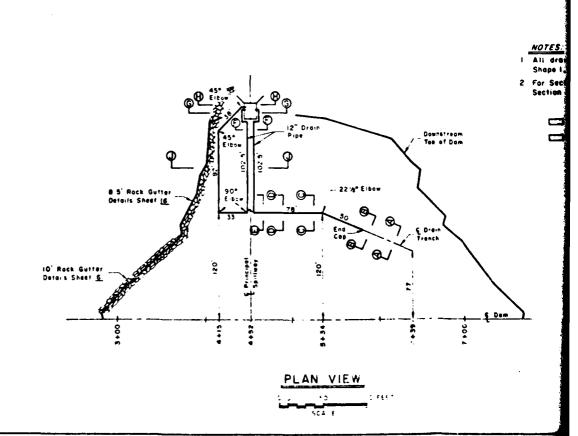
U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

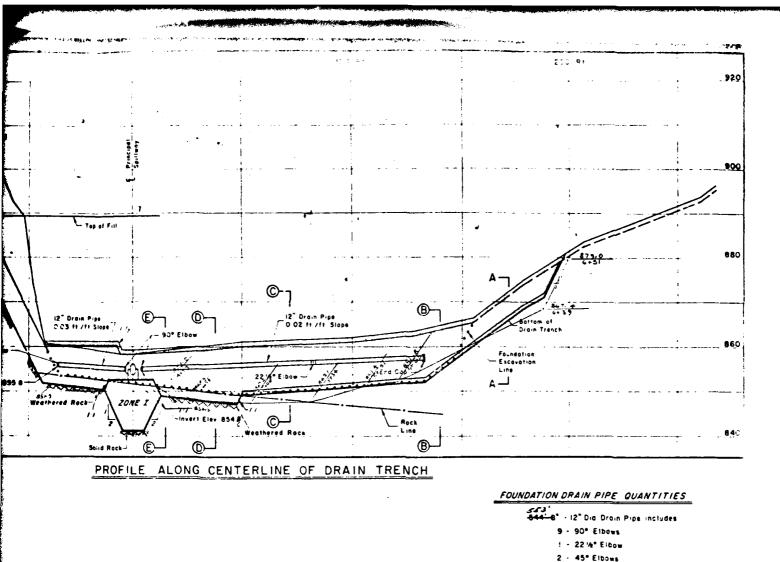
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i chise 5-75

PA-485-P d. Trail







NOTES

- All drain pipe shall be 12" Dia . Class I or II . Shape I, Coating A, 16 Gage, Perforated (Spec 551)
- 2 For Sections A-A thru H-H see sheet 12. Section J-J see sheet 16

Em Fine Droin Fill

Coarse Drain Fill



PLATE 8

3 - Small Animal Guards (Details Sheet 32

1 - Metal End Cap

FINE DRAIN FILL GRADATION LIMITS

	SEIVE	% PASSING (Bosed on Dry Weight)
4	3/8	000
	No 4	90-100
127	No B	70 - 100
1-[No 16	50 - 65
15[No 30	30 - 65
١٥٢	No 50	IC - 30
TOQue	No 100	
	Na-200	< 3

DE LINE TO SERVE HARMON CREEK WATERSHED FLOCOMATER RETARD NO DAY PARAES

WASH NOTON COUNTY, FENNSHIVAN A FOUNDATION DRAINAGE

U.S. DEPARTMENT OF AGRICULTURE

SOIL CONSERVATION SERVICE -41 Mes . 45 8-· ver

9 9 & Drain Tranch **@**_/ € Dom

go rer :

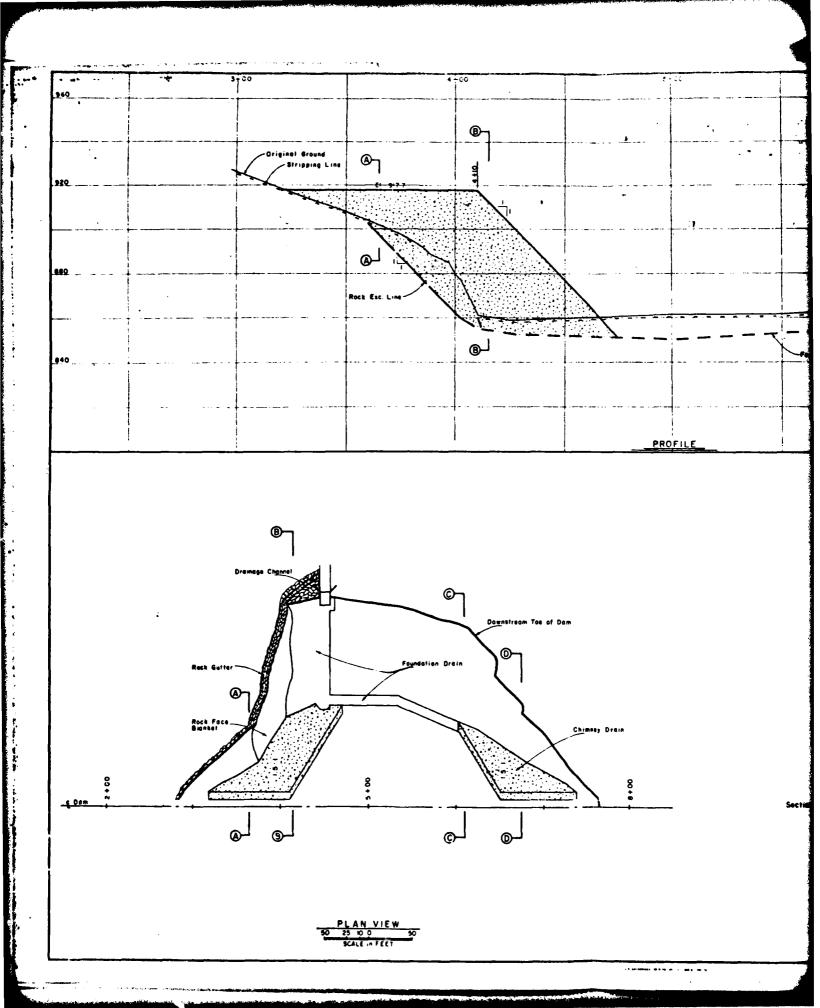
COARSE DRAIN FILL

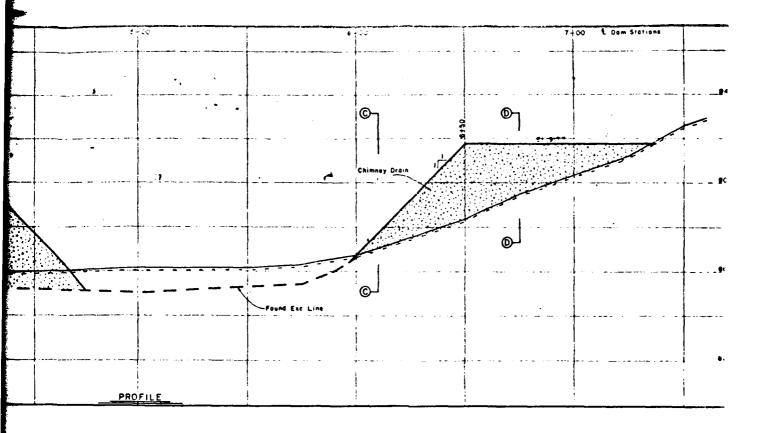
GRADATION LIMITS

	SEIVE NO	% PASSING (Bosed on Dry Weight)
	1 '/2 "	100
اءةا	1 "	90-100
1881	V2	25 - 60
اء <u>۽</u> ا	No 4	0 - 10
No 2	No 8	0 - 5
الستا	No 200	< 3

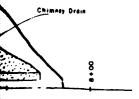
5. 9 7 59 PA-485-P

505-64G-1 4 1844 1-1





5



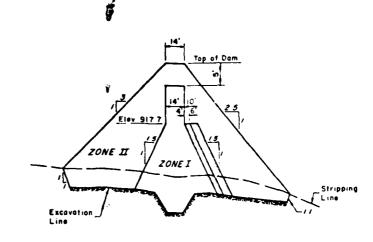
Sections A-A thru 0-0 see shis. 14 8 15

PLATE 9 AS BUILT PLANS

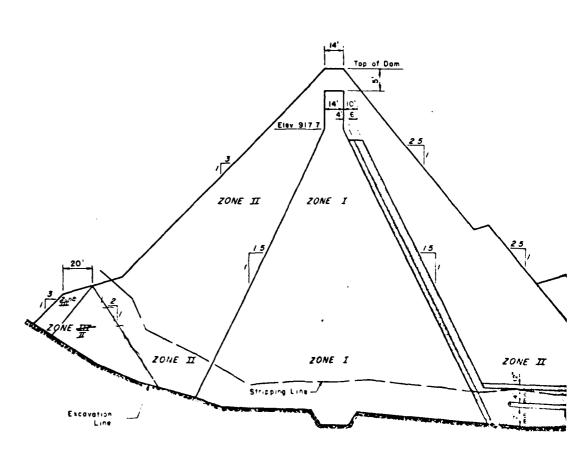
HARMON CREEK WATERSHED
FLOODWATER PETARDING DAN PA-465
WASHINGTON COUNTY, PENNSYLVANIA
CHIMNEY DRAIN
U.S. TUPPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE
A STALTER 4-75
A MAIN YOUR SERVICE PA-485-P

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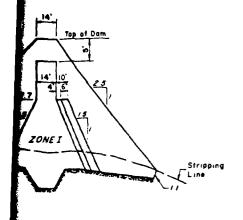
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CROSS-SECTION OF DAM AT & STATION 3+65

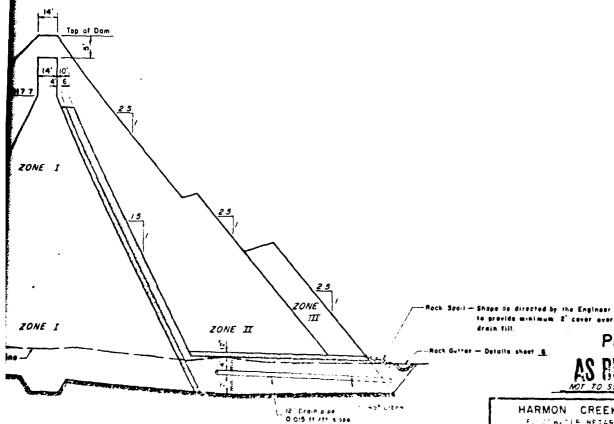


CROSS-SECTION OF DAM AT € STATION 4+15 (SECTION B-B)



DAM AT & STATION 3+65

CTION A-A)



IF DAM AT & STATION 4+15

SECTION B-B)

PLATE 10

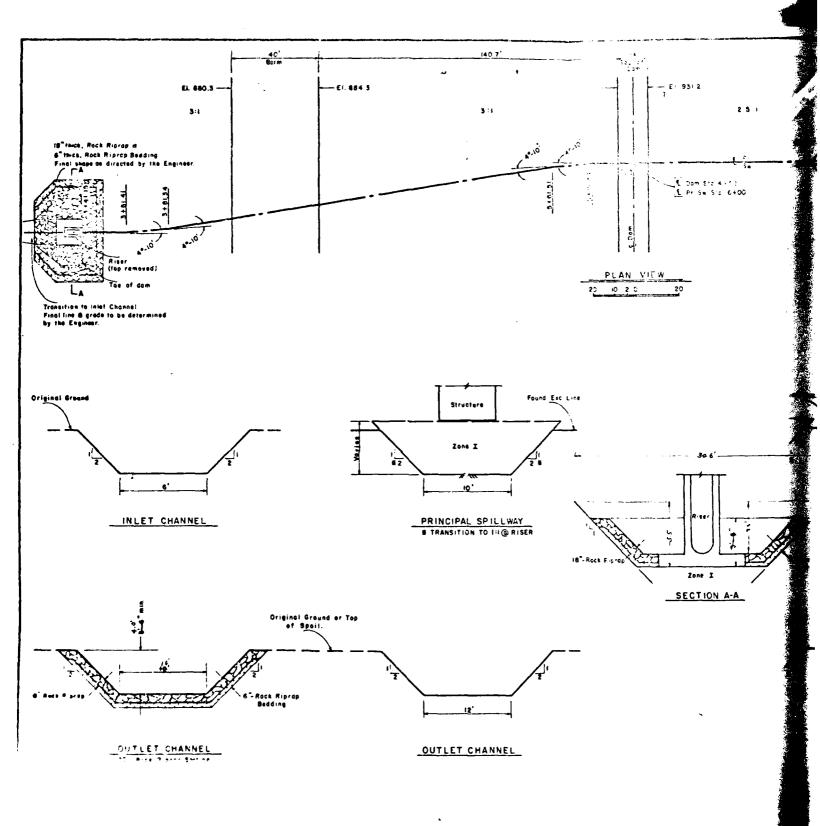
HARMON CREEK WATERSHED FULCTION THE RETARD NO TAM BALLTS ARCHITETT & COUNTY, +0 INS EVANIA CHIMNEY DRAIN (SECTIONS)

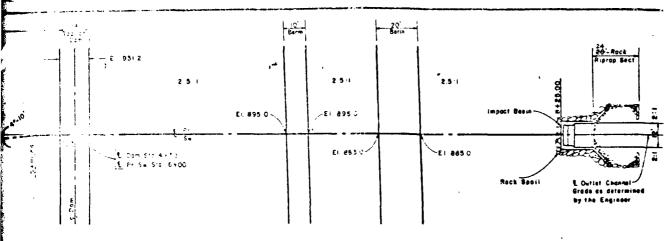
U. S. DEPARTMENT OF AGRICULTUA SOIL CONSERVATION SERVICE

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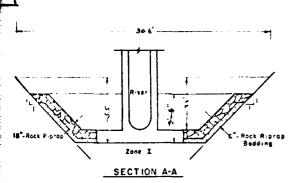
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4. 17° 4 PA-485-





PLAN VIEW 20 10 2 0 20



AS BUILT

D. C. C. 24	
JOINT DIST FROM INVER	EL.
233 322	
2 13.5 \$1.4	
J-3 39.97 355	
52.97	
J-5 139/ E-S	
2:6 3:73 455	4
1.7 . 3.65 8.55	_
J 8 37.57 \$55.0	
1 9 59 49 65 c	
10 7941 555	
111 9933 855	
12 2.3.15 2.54	
3 33	
4 159.83 254	
J-15 278.81 654	
J 6 232 73 854	
2.9.5 454.	
3357 5-1	
J-19 258 49 852	
J20 31541 832	
21 233 33 533	4.3
22 4 8.25 553	
J-23 42592 253	
1.24 -, 45.64 253	
J-25 46576 PSZ	
J-26 485 852	

AS BUILT COLLAR DATA FOR 30" 1 D PIPE

COLLAR	DIST FROM RISER WALL	MYERT ZL
	2.5	
2	45	
3		
4	۵;	
خ	116	L
	- 39.5	
1		
8	168	
9	1	
10	انة	
11	25.5	L
12	28"	
13	3 € .	
/4	220	
15	351	

30° 10. Reinforced Concrete Pressure Pipe Steel Cylinder Type, Spec 541 (AWWA C-301)

4041 - Straight Sections

40' - Bevel Left Sections, 4°-10' (2)

40' - Bevel Right Sections, 4°-10' (2)

f - Spigot Wall Fitting (for 15" wall)

484' - Total (provide with deep joints)

CONSTRUCTION NOTES

- I Outlet end of pipe to be finished so that no metal is exposed
- 2 Pipe layout data to be firnished by the Engineer
- 3 Rock freetment required on exposed rock as directed by the Enginter
- 4 Pran View given for 22 light gards of conduct of infiltengths or other combinations of infiltength are used, revision by a province of renductive sections of a province of the conductive sections.
- 5 Approx became so must gradation limits for time drain fill (sht _ii_)

AS BUILT PLANS

HARMON CREEK WATERSHED FLOORATED RETITIONS DAM DA-485 WASHINGTON COUNTY, PENNSTLVANIA

PRINCIPAL SPILLWAY

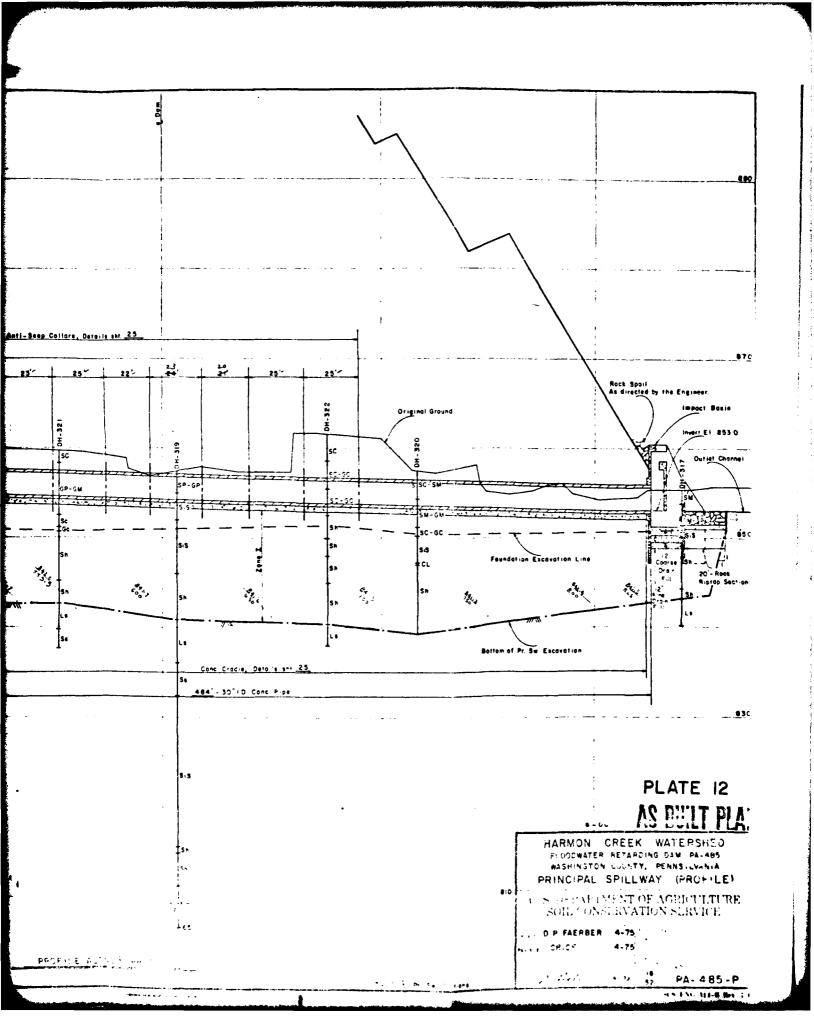
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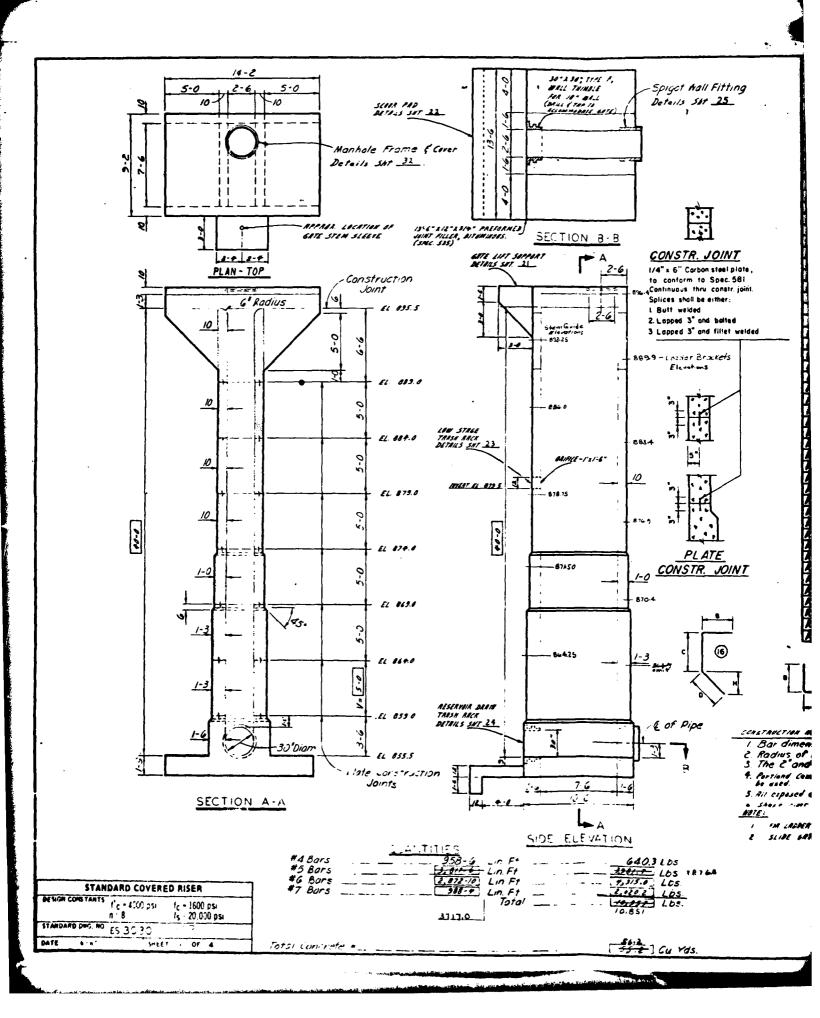
D P FAERBER 3-75

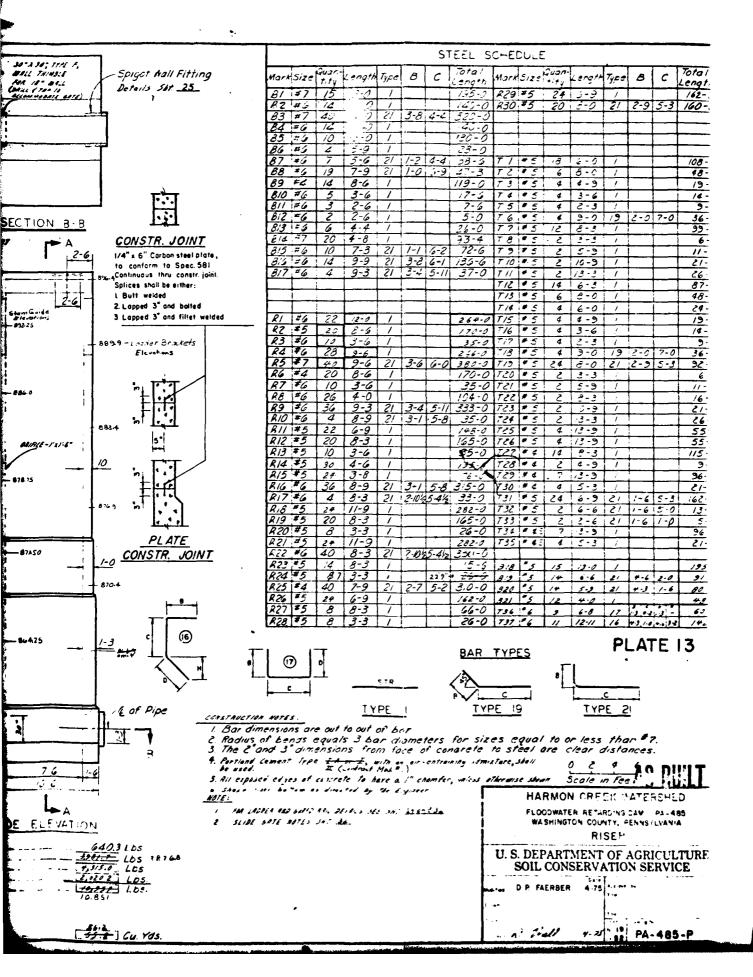
R A Statter 3-75,

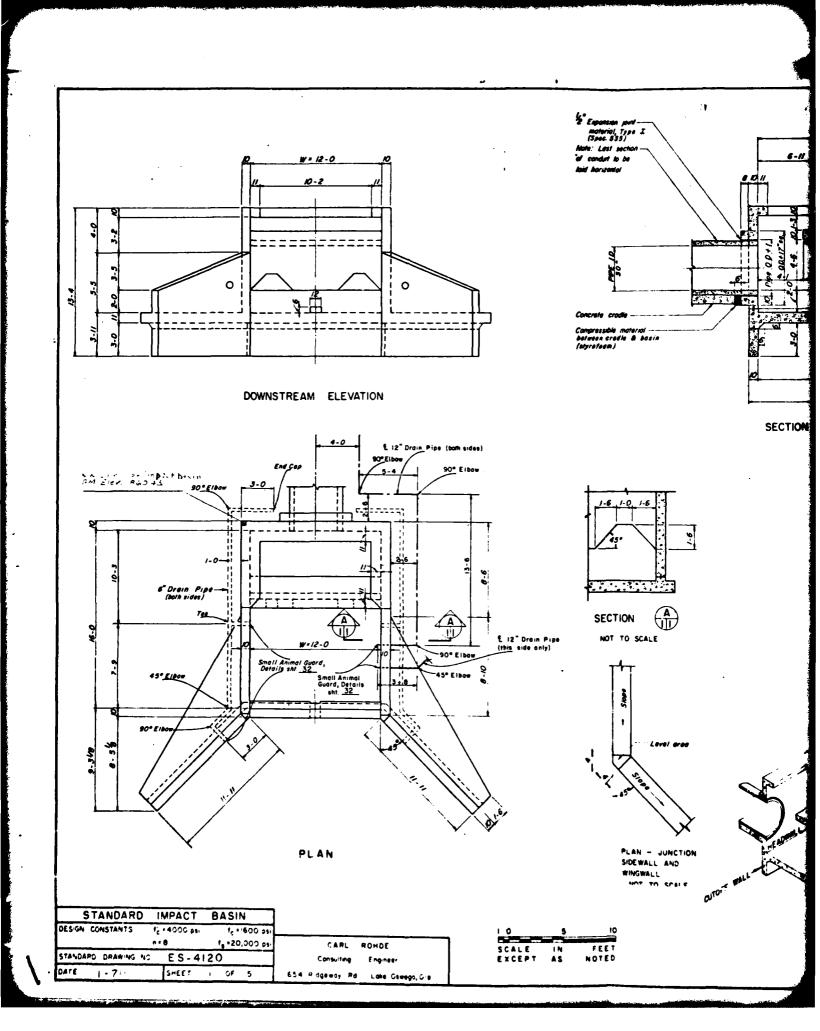
2 1/2 17 PA-485-P

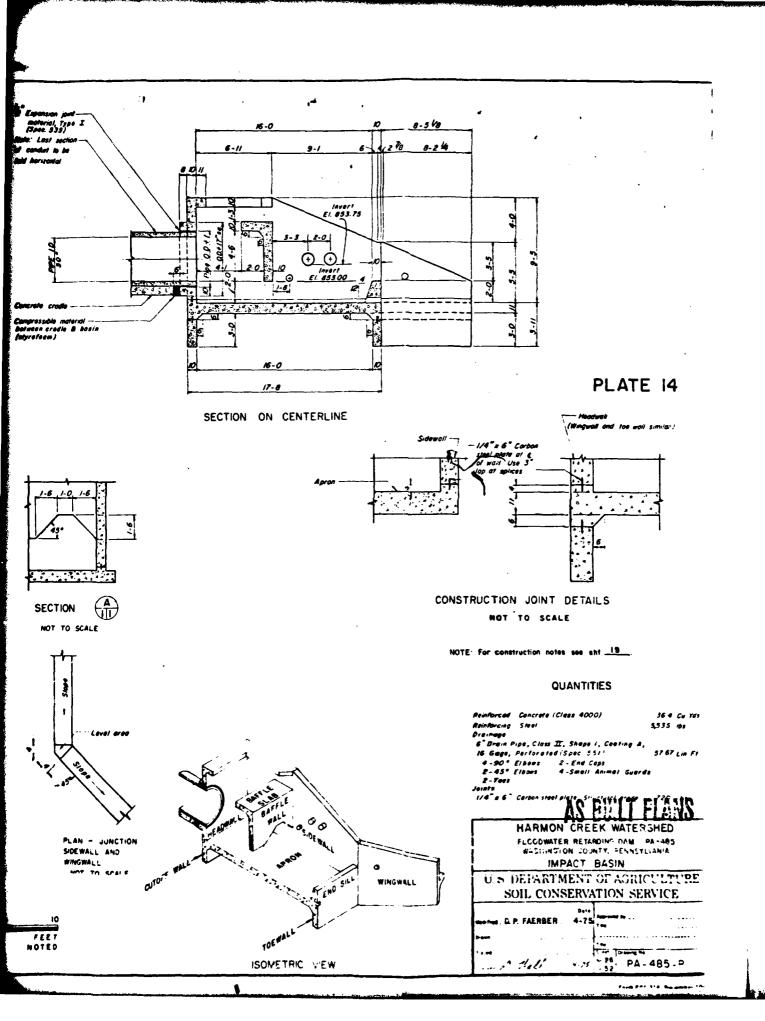
Riser Crest El. 895.5 880 Orifice Crest El. 879.5 Zone III 15 - Conc. Anti-Seep Collars, Details sht 25 573 573 25'
2' min cover rea'd around pipe (Zone I). DH-316 SM-SP Zone I sc-sc 6 Conc Cracie, Details les

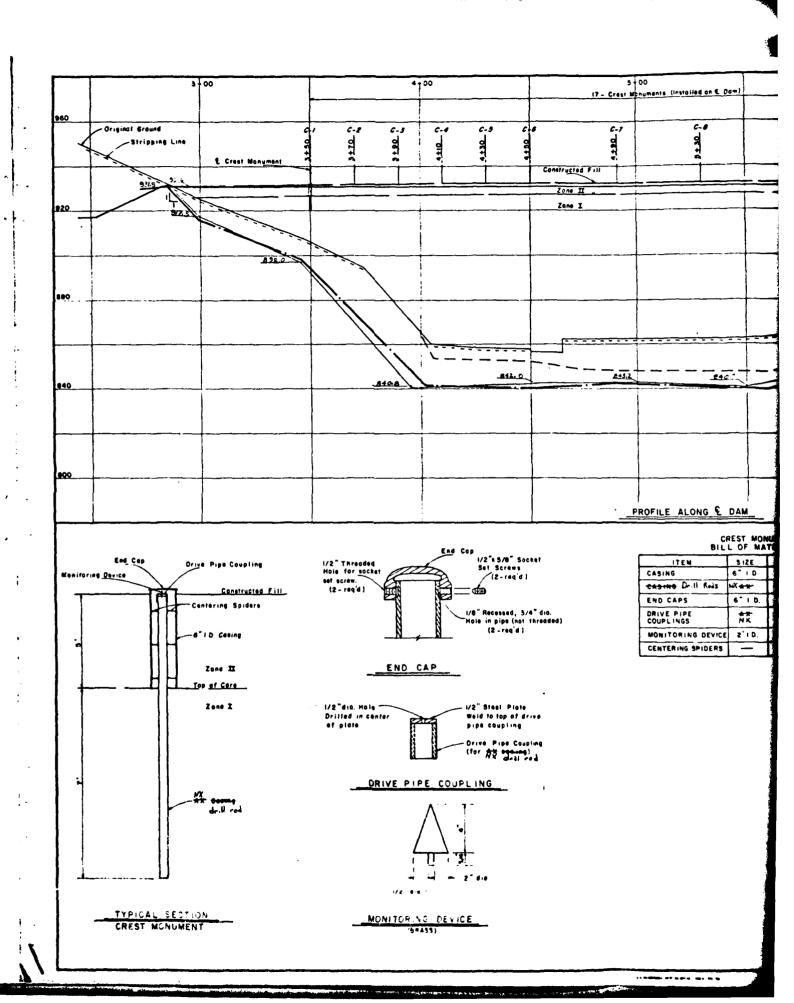


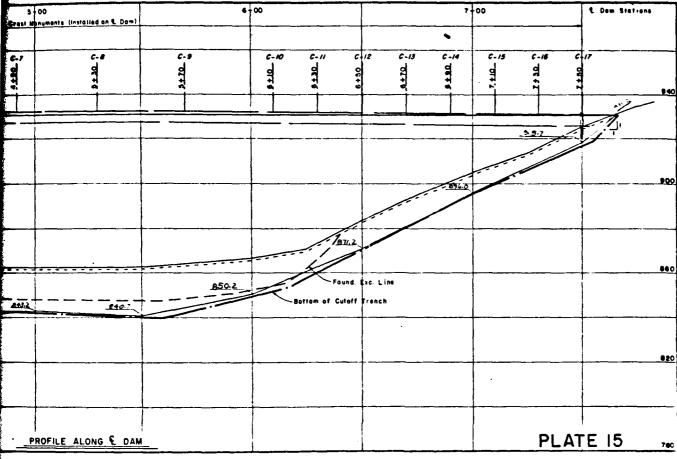












CREST MONUMENT BILL OF MATERIALS

ITEM	SIZE	LENGTH	QUANTITY
CASING	6 10	5' - 0"	17
CASINO Dr.Il Rols	NX++	15'-0"	17
END CAPS	6" I D.		17
DRIVE PIPE COUPLINGS	AX NX		17
MONITORING DEVICE	2"10.		17
CENTERING SPIDERS			As Needed

ŧ

INSTALLATION NOTES:

- 1. 6" dia. casing to be seated to top of core (Zone 1 fill).
- 2. 6" casing to be cleaned out to top of core.
- 3. Flush coupled hi Gaster with flush drive shoe to be centered in 6" casing and driven vertically 7" into core material.
- 4. Standard driving equipment shall be used.
- 5. The contractor shall arrange his activities such that
 - o. Immediately efter installation of such crest monument, the monitoring device shall be installed and elevations of such monument determined to the nearest .01".
- Upon installation of individual crest monaments after Monament 61, the monitoring device shall be installed and the horizontal distance to the previous monament shall be determined to the meanest 0.005".
- 6. All manuments are to be constructed on the centerline of dem
- 7 Crest monument shall be installed true and plumb
- 8 Centering Spiders show be removed after monument installation is complete.
- 9. Moniforing Devises shall be die punched i thru 17

AS PULL PLANS

HARMON CREEK WATERSHED
FLOODWATER RETARDING DAM PA-485
WASHINGTON COUNTY, PENKS (SANIA
CREST MONUMENT INSTALL ATION

U. S. DEPARTMENT OF AGRICULTURE SOU CONSERVATION SERVICE

..... D.P FAERBER 5-75

CRISE

5-75,

1 7/42 5-25 33 PA-485-P

APPENDIX F

REGIONAL GEOLOGY

PA 485 NDI No. PA 01123, PennDER No. 63-81, SCS No. PA 485

REGIONAL GEOLOGY

PA 485 is located in the Pittsburgh Plateaus Section of the Appalachian Plateaus Physiographic Province. Bedrock units below the dam are contained in the Glenshaw formation of the Conemaugh group, Pennsylvanian system. The Glenshaw formation consists of cyclic sequences of sandstone, shale, red beds, and thin limestone and coal; several fossiliferous limestone; and Ames limestone bed at the top of the formation. base of the Ames limestone is exposed in the emergency spillway cut approximately at Elevation 925 feet M.S.L. Above the Ames limestone on the valley walls is the Casselman formation of the Conemaugh group. This formation consists of cyclic sequences of sandstone, shale, red beds, and thin limestone and coal. Immediately below the Ames limestone is a unit known as the "Pittsburgh Red Beds" which consists of greenish-gray, red, and variegated clay shales. This unit has been known to cause landslide problems in the Pittsburgh Region.

The Pittsburgh coal was projected at approximate Elevation 1150 feet M.S.L. or 219 feet above the top of the dam. Subsequent to the site investigation and soil mechanics testing for this site by the SCS, strip mine spoil ranging in thickness from approximately 2 to 4 feet was spread over the borrow area on top of the left abutment. This mining activity and other strip mining activity in the watershed area were mining the Pittsburgh coal. (Note: from the information available it is estimated that this strip mine spoil was used as zone II material in the embankment.)

The left abutment of the dam was composed of thin to thick bedded, weathered, moderately soft, shaly siltstone. This abutment was nearly vertical originally and was cut back to 1H: 1V during construction. The siltstone excavated was placed as a rockfill buttress on both the upstream and downstream slopes. On the right abutment, residual and colluvial soils overlie the weathered shaly and sandy siltstone. In the floodplain, alluvium of silty clay (CL) originally extended to a depth of 4.0 feet. Below the CL material was a clayey gravel (GC) to a depth of 9.0 feet. Blow counts in this material ranged from 6 to 7 blows per foot during the original drilling program. Below 7 feet to 29 feet is residual or colluvial sandy clay (CL) with strata of clayey gravel (GC). This material had blow counts ranging from 26 to 69 blows per foot. During construction of the dam the upper 9.0 feet of valley alluvium was removed prior to placing embankment material.

A regional geology map and legend are presented on the following pages. Additional site geology can be obtained by reviewing the "Detailed Geologic Investigation Report" in the SCS design folder for this dam.

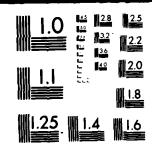


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NATIONAL DAM SAFETY PROGRAM. UNNAMED TRIBUTARY TO HARMON CREEK, --TC(U)
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MICROCOPY RESOLUTION TEST CHART

GEOLOGY MAP LEGEND

GROUP FORMATION

DESCRIPTION

<u> </u>	Alluvium		Sand, gravel, clay.
Terrace deposits		Q1	Sand, clay, gravel on terraces above present rivers; includes Carmichaels Formation.
DUNKARD	Greene		Cyclic sequences of sandstone, shale, red beds, thin limestones and coals.
	Washington	Pw	Cyclic sequences of sandstone, shale, limestone, and coal; contains Washington coal bed at base.
	Waynesburg	and the second of the second	Cyclic sequences of sandstone, shale, limestone and coal; contains Waynesburg coal bed at base.
MONONGAHELA		3	Cyclic sequences of shale, limestone, sandstone and coal; contains Pittsburgh coal bed at base.
P. CONEMAUGH	Casselman	I Pcc	Cyclic sequence of sandstone, shale, red beds and thin limestone and coal.
	Ames		
	Glenshaw	Pcg	Cyclic sequences of sandstone, shale, red beds and thin limestone and coal; several fossiliferous limestone; Ames limestone bed at top.
ALLEGHENY	Vanport —	Pa	Cyclic sequences of shale, sandstone, limestone, and coal; contains Brookville coal at base and Upper Freeport coal at top; within group are the commercial Vanport limestone and Kittanning and Clarion coals.
		Pa	
POTTSVILLE			Sandstone and shale; contains some conglomerate and locally mineable coal,
Mauch Chunk			Red and green shale with some sandstone; contains Wymps Gap and Lovalhanna lime – stones.
Pocono			Sandstone and shale with Burgoon sandstone at top.